

ME 233 Advanced Control II

Lecture 18

Stability Analysis Using The Hyperstability Theorem

Adaptive Control

Basic Adaptive Control Principle

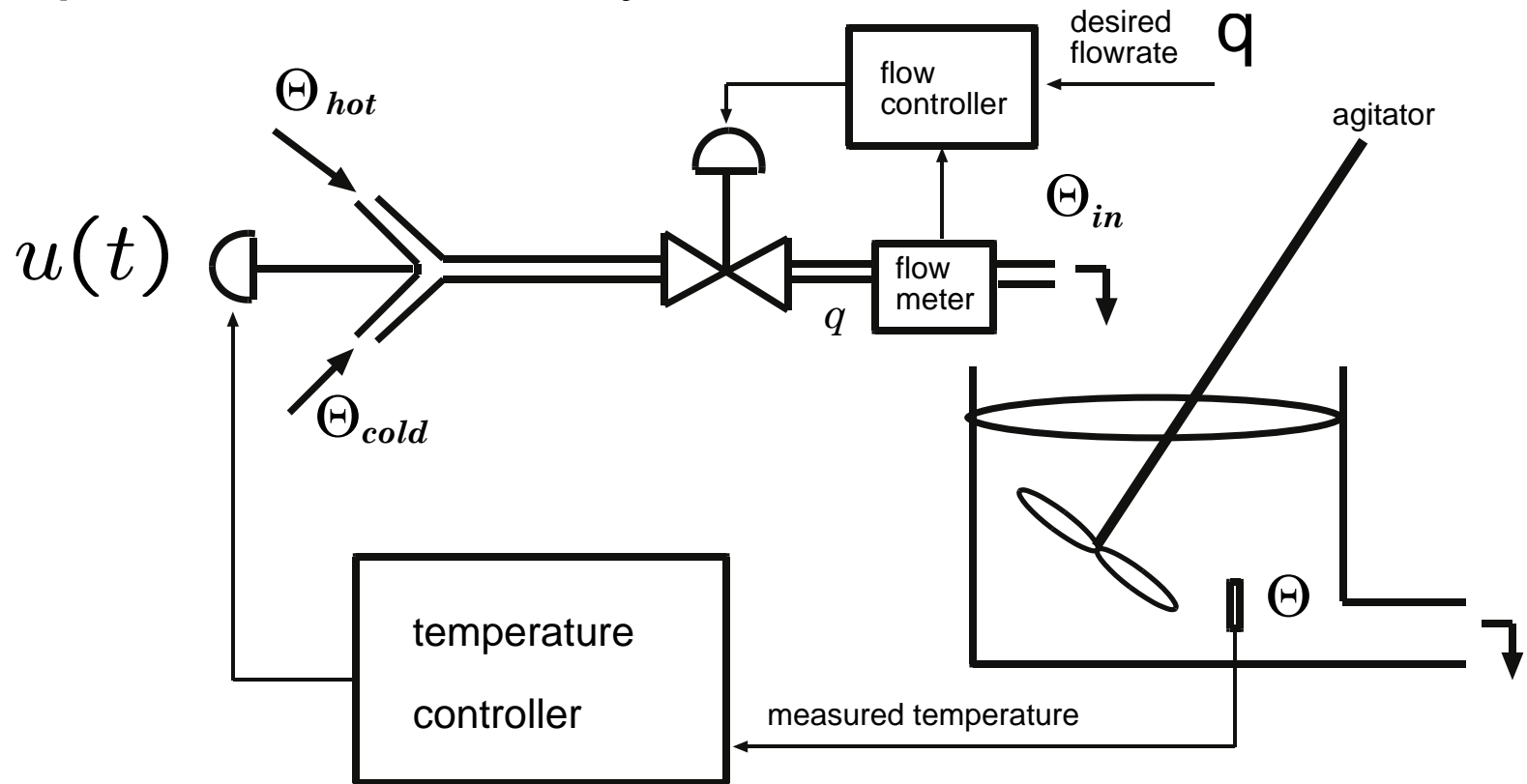
Controller parameters **are not constant**, rather, they are adjusted in an online fashion by a ***Parameter Adaptation Algorithm (PAA)***

When is adaptive control used?

- Plant parameters are unknown
- Plant parameters are time varying

Example of a system with varying parameters

- Temperature control system

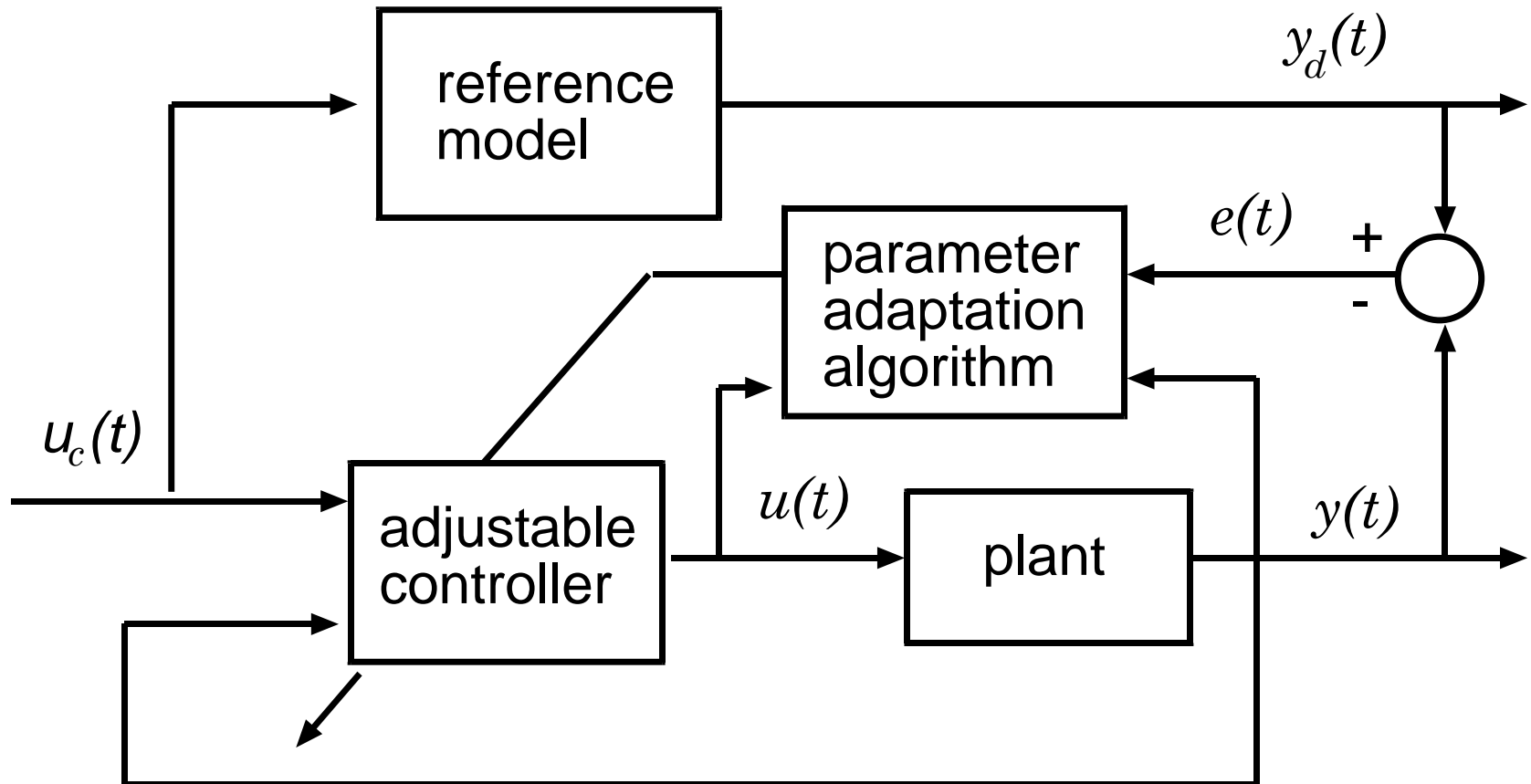


$$\frac{d}{dt}\theta(t) = - \underbrace{\frac{q}{V}}_{a(q)} \theta(t) + \underbrace{\frac{kq}{V}}_{b(q)} u(t - t_d)$$

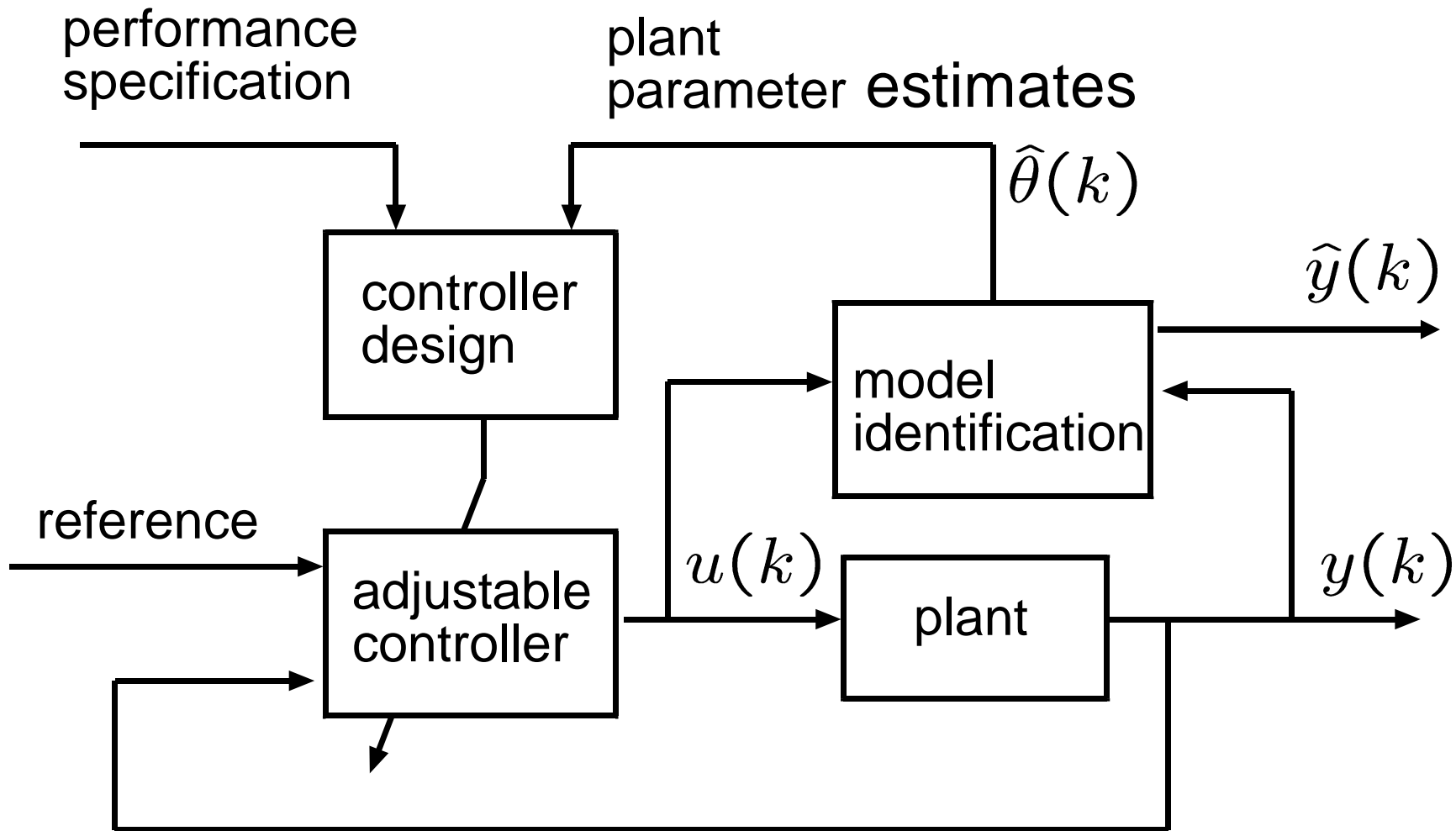
Adaptive Control Classification

- Continuous time VS **discrete time**
- Direct VS indirect
- MRAS VS **STR**

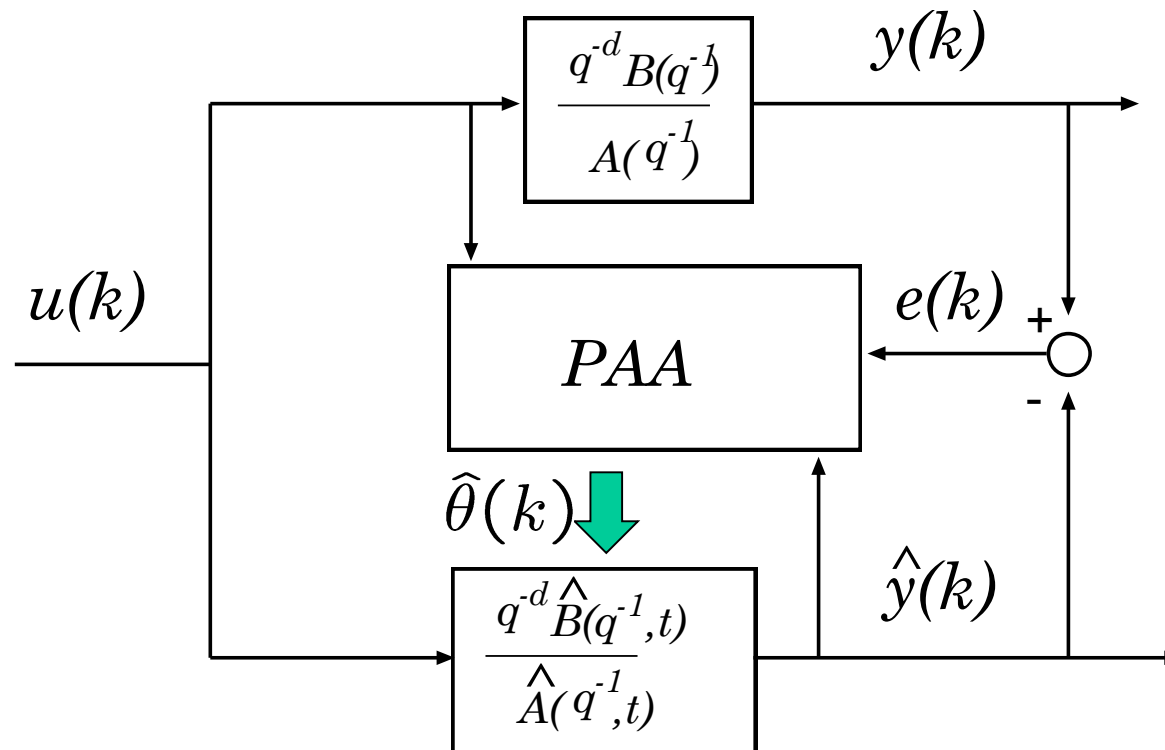
Model Reference Adaptive Systems (MRAS)



Self-Tuning Regulators (STR)

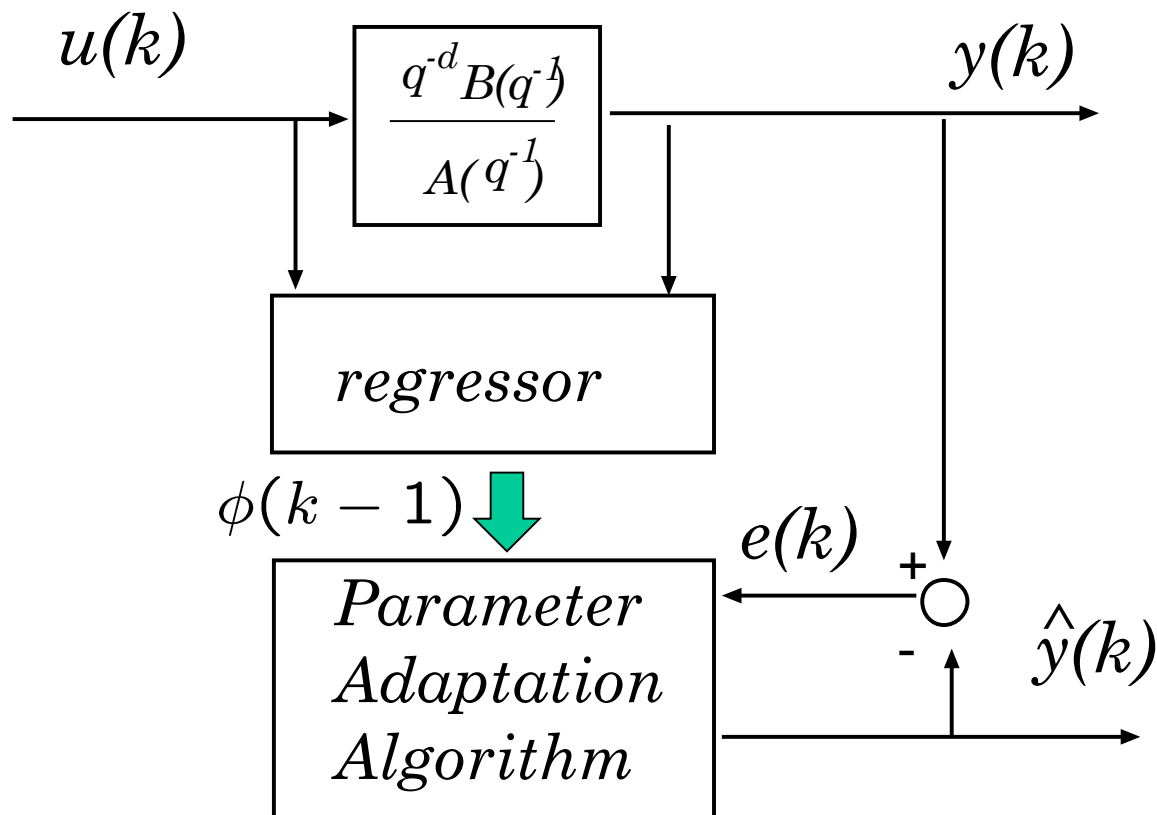


Identification of a LTI system



Parallel model

Identification of a LTI system



Series-parallel model

(We will use this model throughout this lecture)

Plant ARMA Model

Plant model

$$A(q^{-1})y(k) = q^{-d}B(q^{-1})u(k)$$

where

$$A(q^{-1}) = 1 + a_1q^{-1} + \dots + a_nq^{-n}$$

$$B(q^{-1}) = b_o + b_1q^{-1} + \dots + b_mq^{-m}$$

***Unknown* plant parameters**

Assume ARMA model parameters are unknown

$$y(k) = - \underline{a_1} y(k-1) \cdots - \underline{a_n} y(k-n) \\ + \underline{b_0} u(k-d) \cdots + \underline{b_m} u(k-d-m)$$

Define:

$$\theta = \left[\underline{a_1} \quad \cdots \quad \underline{a_n} \quad \underline{b_0} \quad \cdots \quad \underline{b_m} \right]^T$$

As the unknown parameter vector

Regressor vector

Collect all measurable signals in one vector

$$y(k) = - a_1 \underline{y(k-1)} \cdots - a_n \underline{y(k-n)} \\ + b_0 \underline{u(k-d)} \cdots + b_m \underline{u(k-d-m)}$$

We define

$$\phi(k-1) = \left[\underline{-y(k-1) \cdots -y(k-n)} \right. \\ \left. \underline{u(k-d) \cdots u(k-d-m)} \right]^T$$

as the **known** regressor vector

Plant ARMA Model

Plant model

$$y(k) = \phi^T(k-1) \theta$$

where

$$\theta = \begin{bmatrix} a_1 & \cdots & a_n & b_0 & \cdots & b_m \end{bmatrix}^T$$

$$\phi(k-1) = \begin{bmatrix} -y(k-1) & \cdots & -y(k-n) \\ u(k-d) & \cdots & u(k-d-m) \end{bmatrix}^T$$

Plant ARMA Model

Plant estimate (series-parallel)

$$\hat{y}(k) = \phi^T(k-1) \hat{\theta}(k)$$

where

$$\hat{\theta}(k) = \left[\hat{a}_1(k) \quad \cdots \quad \hat{a}_n(k) \quad \hat{b}_o(k) \quad \cdots \quad \hat{b}_m(k) \right]^T$$

$$\phi(k-1) = \left[-y(k-1) \quad \cdots \quad -y(k-n) \right. \\ \left. u(k-d) \quad \cdots \quad u(k-d-m) \right]^T$$

Plant output estimate

Plant a-posteriori estimate

$$\hat{y}(k) = \phi^T(k-1) \hat{\theta}(k)$$

Plant a-priori estimate

$$\hat{y}^o(k) = \phi^T(k-1) \hat{\theta}(k-1)$$

Plant a-posteriori error

$$y(k) = \phi^T(k-1) \theta$$

$$\hat{y}(k) = \phi^T(k-1) \hat{\theta}(k)$$

error:
$$e(k) = y(k) - \hat{y}(k)$$

$$e(k) = \phi^T(k-1) [\theta - \hat{\theta}(k)]$$

$$= \phi^T(k-1) \tilde{\theta}(k)$$

$$\tilde{\theta}(k) = \theta - \hat{\theta}(k)$$

A Parameter Adaptation Algorithm

PAA

$$F = F^T \succ 0$$

$$\hat{\theta}(k) = \hat{\theta}(k-1) + F \phi(k-1)e(k)$$

Parameter error update law: $\tilde{\theta}(k) = \theta - \hat{\theta}(k)$

$$\tilde{\theta}(k) = \tilde{\theta}(k-1) - F \phi(k-1)e(k)$$

Adaptation Dynamics

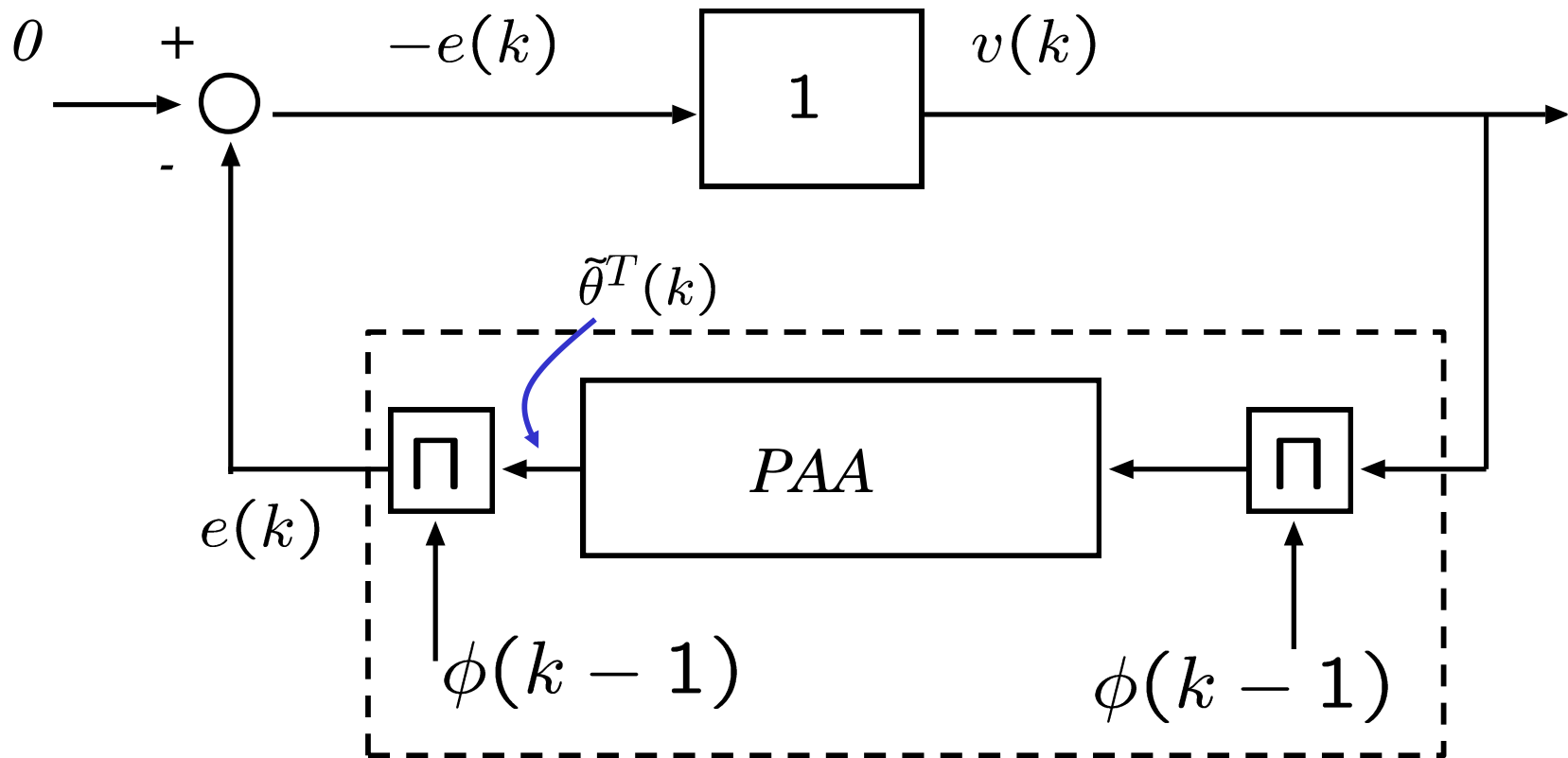
a-posteriori error: $e(k) = y(k) - \hat{y}(k)$

$$e(k) = \phi^T(k-1)\tilde{\theta}(k)$$

Parameter error update law: $\tilde{\theta}(k) = \theta - \hat{\theta}(k)$

$$\tilde{\theta}(k) = \tilde{\theta}(k-1) - F \phi(k-1)e(k)$$

Adaptation Dynamics



$PAA:$
$$\tilde{\theta}(k) = \tilde{\theta}(k-1) + F \phi(k-1)v(k)$$

Convergence of Adaptive Systems

Adaptive systems are nonlinear

We need to prove that the algorithms converge:

- **Output error convergence**

$$e(k) \rightarrow 0$$

$$e(k) = y(k) - \hat{y}(k)$$

- **Parameter error convergence**

$$\tilde{\theta}(k) \rightarrow 0$$

$$\tilde{\theta}(k) = \theta - \hat{\theta}(k)$$

Output error Convergence

Our first goal will be to prove the asymptotic convergence of the output error:

$$e(k) \rightarrow 0$$

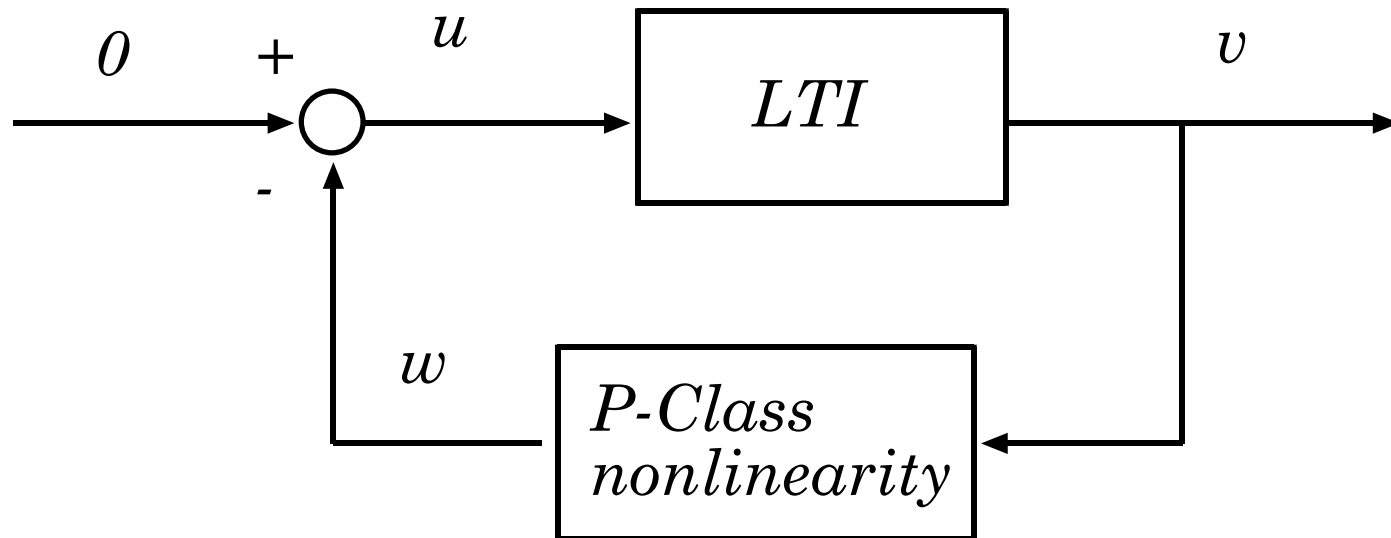
Two frequently used methods of stability analysis are:

- **Stability analysis using Lyapunov's direct method**
 - State space approach
- **Stability analysis using the Passivity or Hyperstability theorems**
 - Input/output approach

Hyperstability

Hyperstability Theory

- Developed by V.M. Popov to analyze the stability of a class of feedback systems (monograph published in 1973)

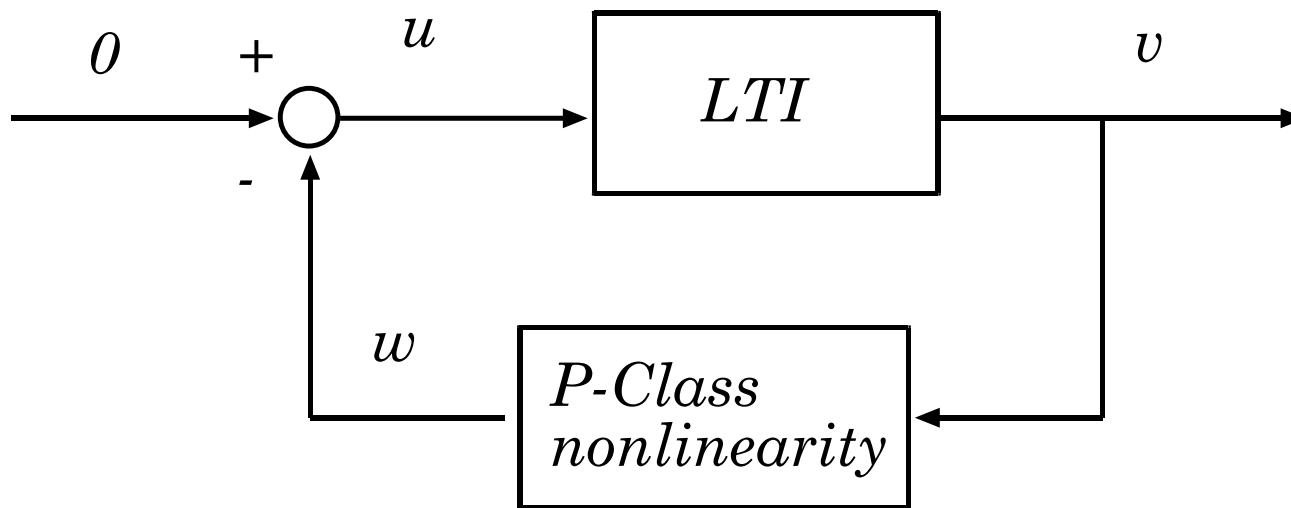


- Popularized by I.D. Landau for the analysis of adaptive systems (first book published in 1979)

Hyperstability Theory

Hyperstability Theory

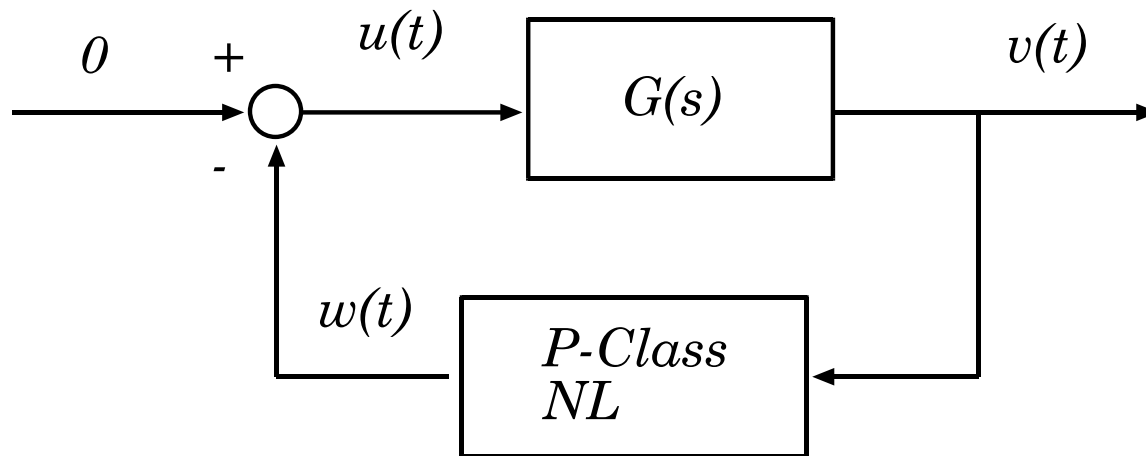
- Applies to both continuous time and discrete time systems



- **Abuse of notation:** We will denote the LTI block by its transfer function

CT Hyperstability Theory

$$G(s) = C(sI - A)^{-1}B + D$$

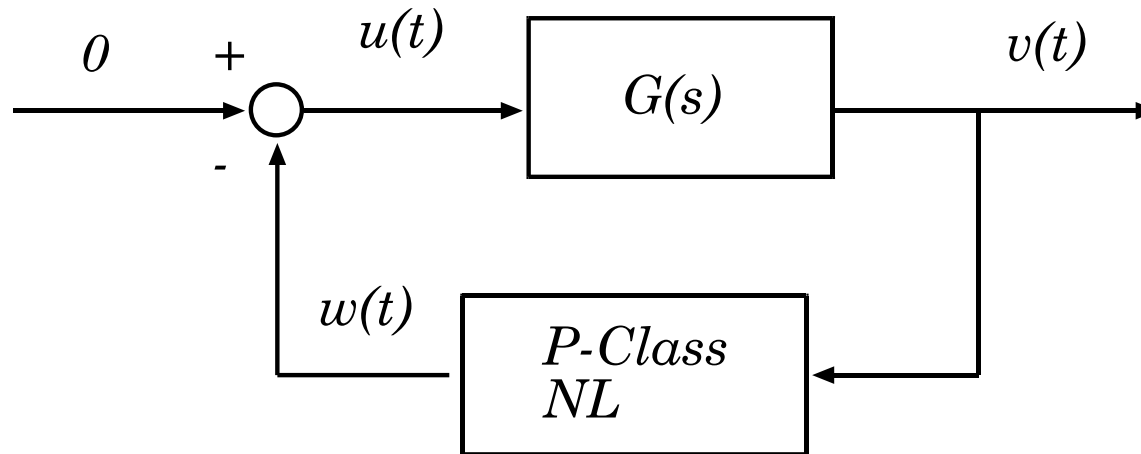


- A state space description of the LTI Block:

$$\frac{d}{dt}x(t) = Ax(t) + Bu(t)$$

$$v(t) = Cx(t) + Du(t)$$

CT Hyperstability Theory

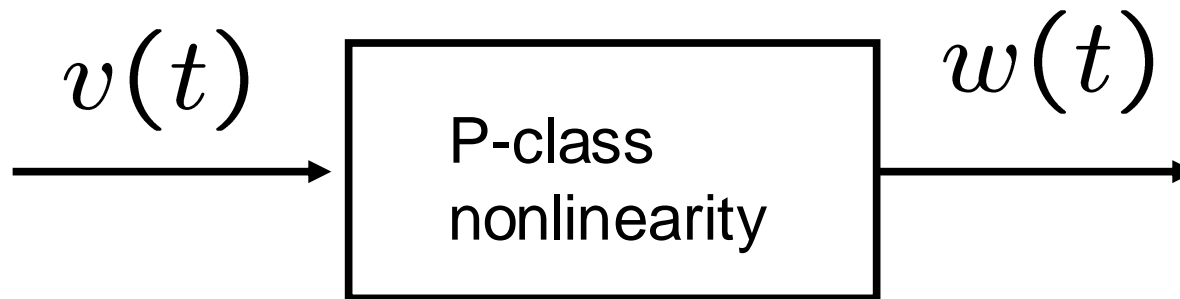


- P-class nonlinearity: (passive nonlinearities)

$$\int_0^t w^T v \, d\tau \geq -\gamma_o^2 \quad \forall t \geq 0$$

Where γ_o is a constant which is a function of the initial conditions

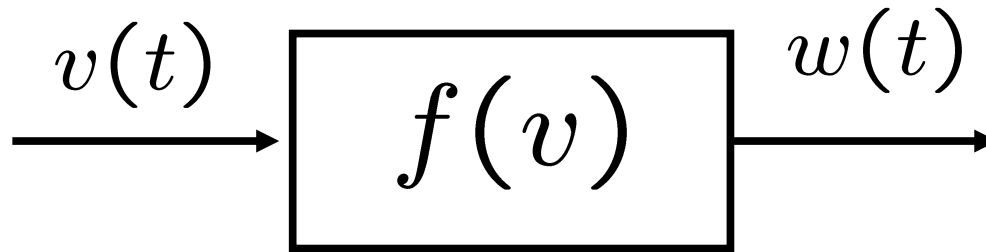
CT Hyperstability Theory



$$\int_0^t w^T v d\tau \geq -\gamma_0^2 \quad \forall t \geq 0$$

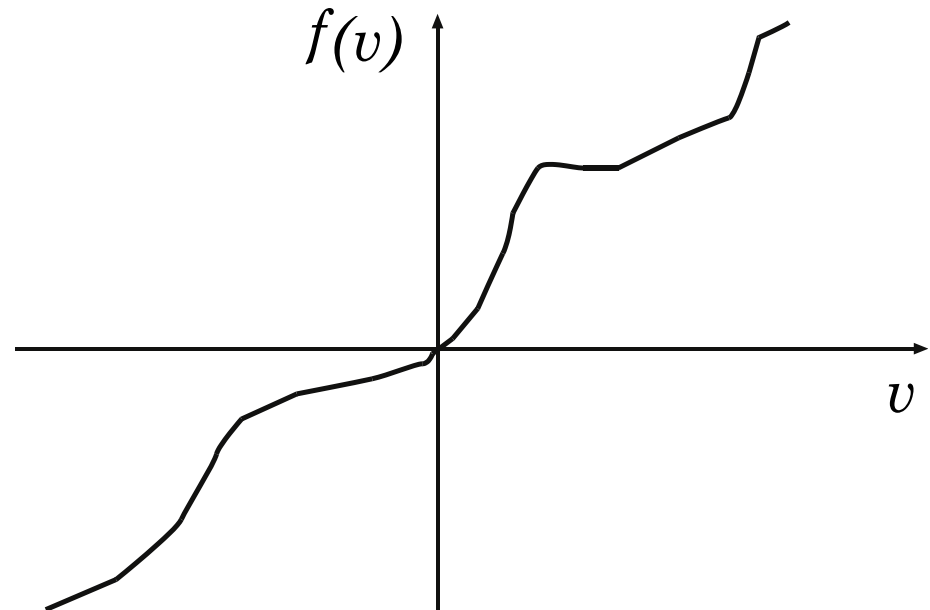
Where γ_0 is a constant which is a function of the initial conditions

Example: Static P-class NL



$$w = f(v)$$

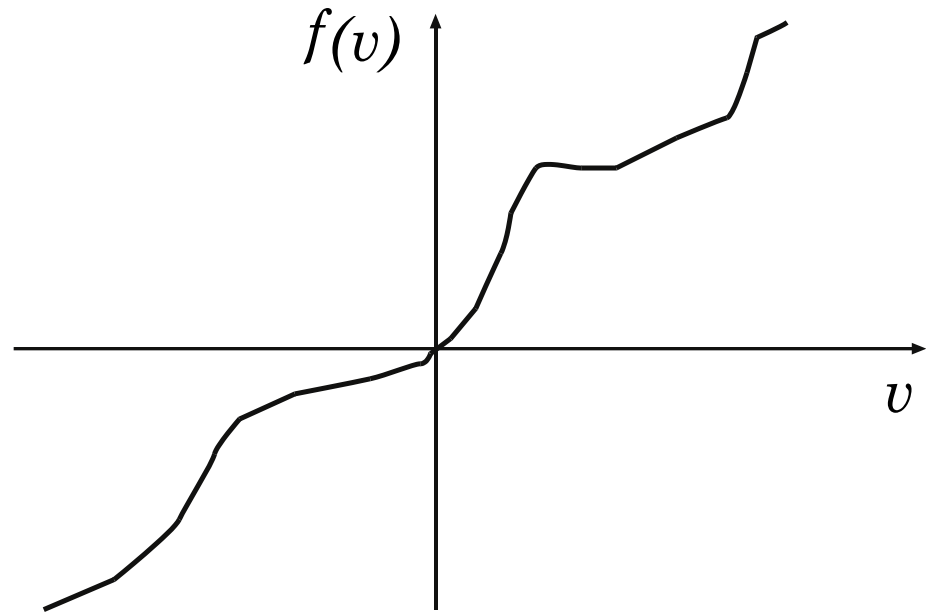
$$v f(v) \geq 0$$



Example: Static P-class NL

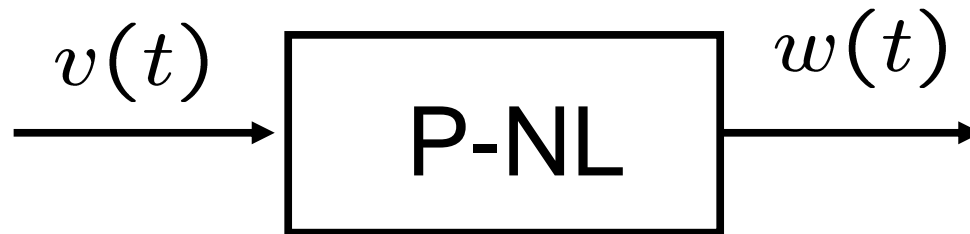
$$w = f(v)$$

$$v f(v) \geq 0$$



$$\int_0^t wv \, d\tau = \int_0^t \underbrace{f(v)v}_{\geq 0} \, d\tau \geq 0 > -\gamma_o^2$$

Example: Dynamic P-class block



$$\left\{ \begin{array}{l} \frac{d}{dt} \tilde{\theta}(t) = F \phi(t) v(t) \\ w(t) = \phi^T(t) \tilde{\theta}(t) \end{array} \right. \quad \begin{array}{l} \phi(t) \in \mathcal{R}^n \\ \tilde{\theta}(0) \in \mathcal{R}^n \\ |\tilde{\theta}(0)| < \infty \\ |\phi(t)| < \infty \end{array}$$

$$F = F^T \succ 0$$

Example: Dynamic P-class block

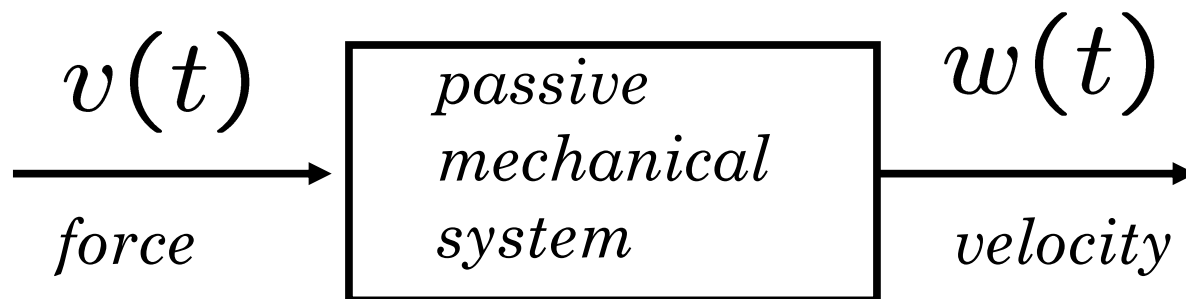
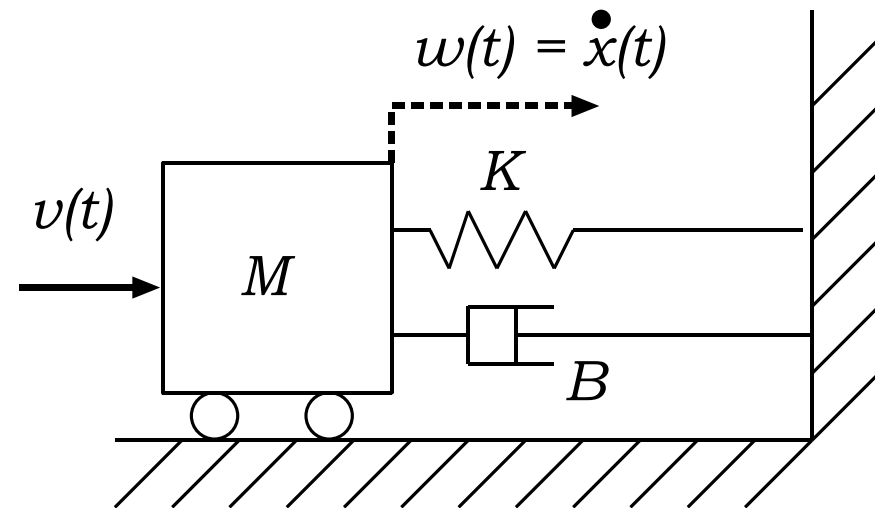
$$w(t) = \phi^T(t) \tilde{\theta}(t) \qquad \dot{\tilde{\theta}}(t) = F \phi(t) v(t)$$

$$\begin{aligned} \int_0^t w(\tau) v(\tau) d\tau &= \int_0^t \phi^T(\tau) \tilde{\theta}(\tau) v(\tau) d\tau \\ &= \int_0^t \tilde{\theta}^T(\tau) \underbrace{[\phi(\tau) \tilde{v}(\tau)]}_{F^{-1} \dot{\tilde{\theta}}(\tau)} d\tau \\ &= \frac{1}{2} \int_0^t \frac{d}{d\tau} \left\{ \tilde{\theta}^T(\tau) F^{-1} \tilde{\theta}(\tau) \right\} d\tau \\ &= \frac{1}{2} \tilde{\theta}^T(t) F^{-1} \tilde{\theta}(t) - \underbrace{\frac{1}{2} \tilde{\theta}^T(0) F^{-1} \tilde{\theta}(0)}_{\gamma_o^2} \\ &\geq -\gamma_o^2 \end{aligned}$$

Example: Passive mechanical system

Input is force and output is velocity

$$M\dot{w} + Bw + Kx = v$$



Example: Passive mechanical system

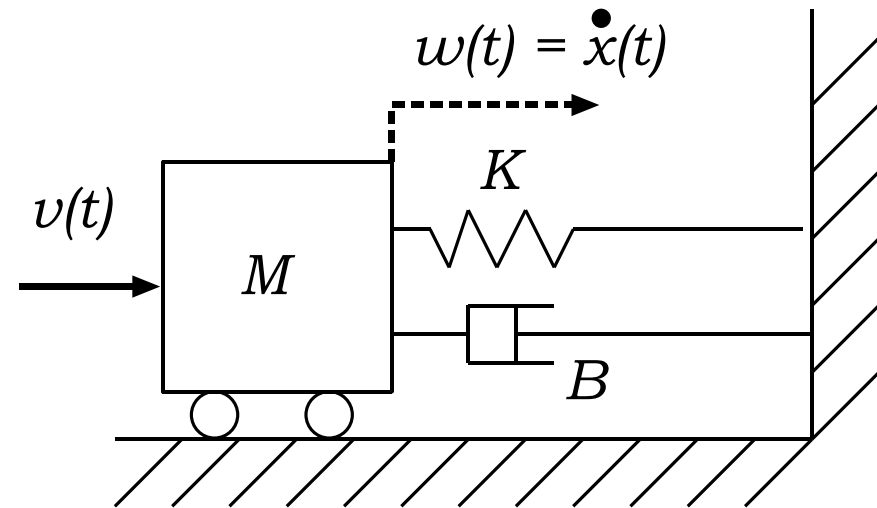
Input is force and output is velocity

$$M\dot{w} + Bw + Kx = v$$

$$\dot{x} = w$$

System Energy:

$$E(t) = \frac{1}{2}Mw^2(t) + \frac{1}{2}Kx^2(t) \geq 0$$

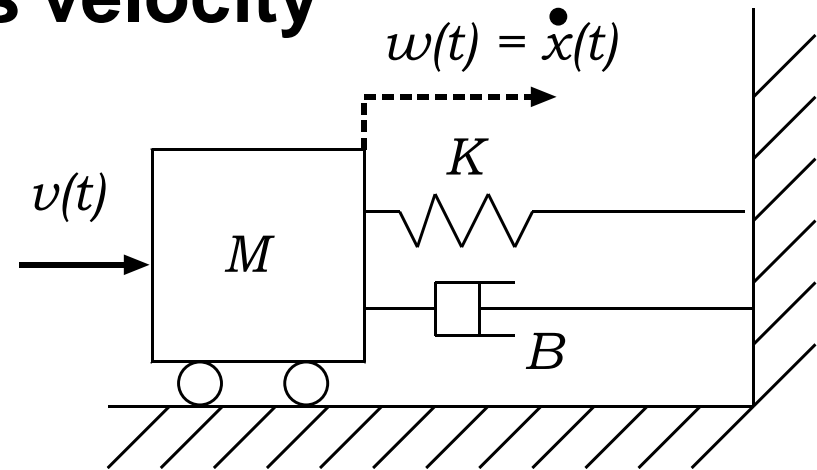


Example: Passive mechanical system

Input is force and output is velocity

$$E(t) = \frac{1}{2}Mw^2(t) + \frac{1}{2}Kx^2(t) \geq 0$$

Differentiating energy



$$\dot{E} = M\dot{w}w + Kxw$$

$$= [-Kx - Bw + v]w + Kxw$$

$$= -\cancel{Kxw} - Bw^2 + wv + \cancel{Kxw}$$

Example: Passive mechanical system

Input is force and output is velocity

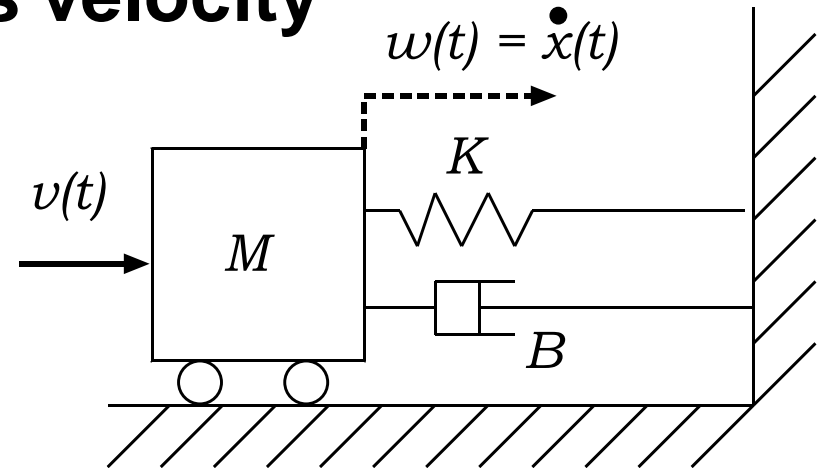
$$E(t) = \frac{1}{2}Mw^2(t) + \frac{1}{2}Kx^2(t) \geq 0$$

Differentiating energy

$$\dot{E} = -Bw^2 + wv$$

$$\underbrace{wv}_{\text{power input}} = \dot{E} + Bw^2$$

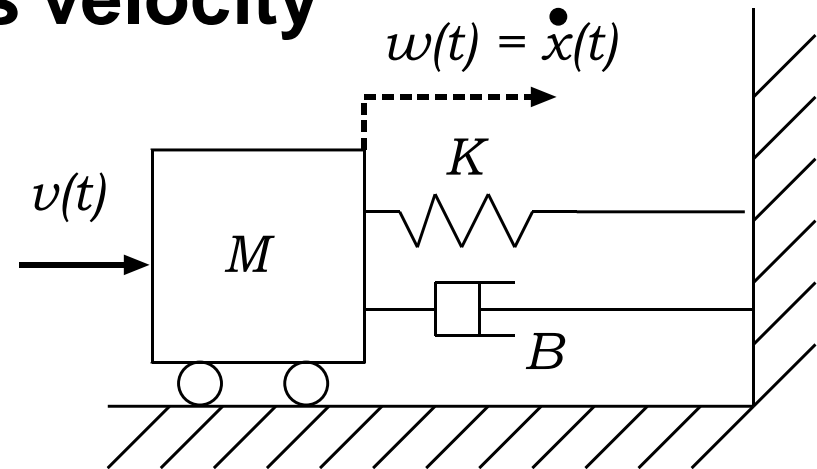
power input



Example: Passive mechanical system

Input is force and output is velocity

$$E(t) = \frac{1}{2}Mw^2(t) + \frac{1}{2}Kx^2(t) \geq 0$$



integrating power,

$$\int_0^t wv \, d\tau = E(t) - E(0) + \int_0^t Bw^2(\tau) \, d\tau$$

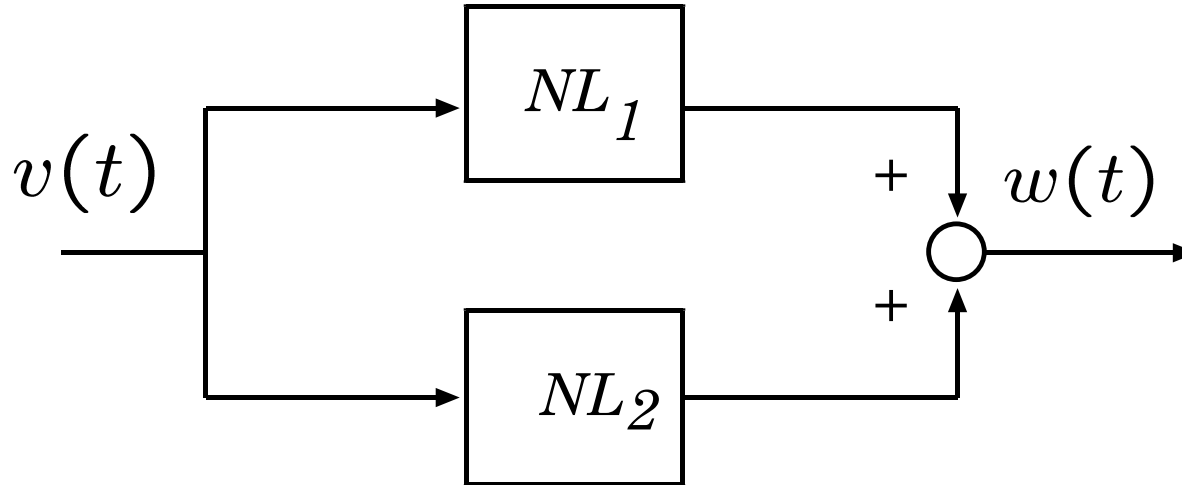
$$\geq -\gamma_0^2$$

$$\gamma_0^2 = E(0) \geq 0$$

Examples of P-class NL

Lemma:

- The parallel combination of two P-class nonlinearities is also a P-class nonlinearity.

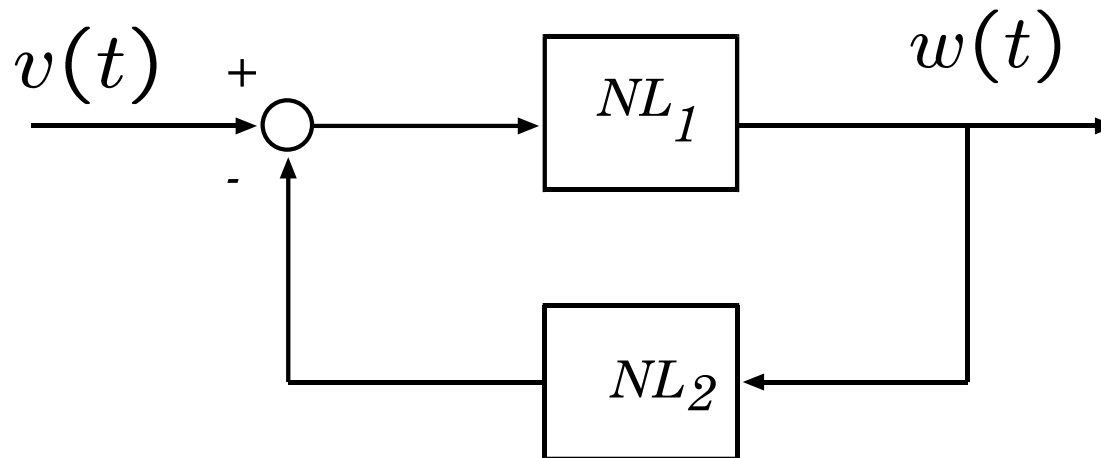


$$\int_0^t w^T v d\tau \geq -\gamma_o^2$$

Examples of P-class NL

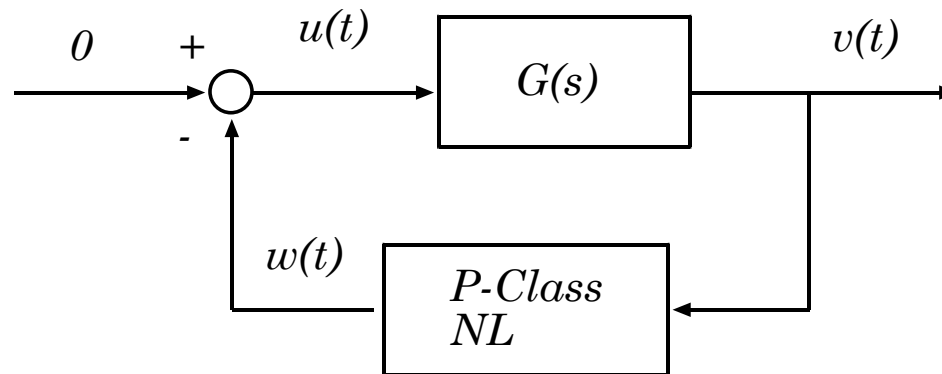
Lemma:

- The feedback combination of two P-class nonlinearities is also a P-class nonlinearity.



$$\int_0^t w^T v d\tau \geq -\gamma_o^2$$

CT Hyperstability

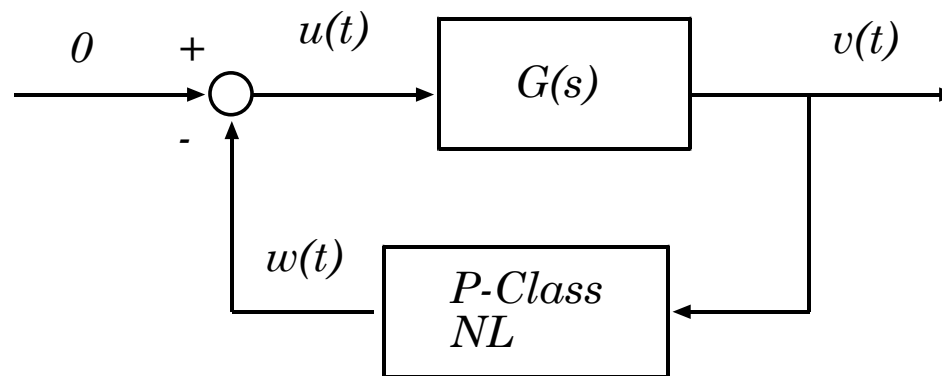


Hyperstability: The above feedback system is hyperstable if there exist positive bounded constants δ_1, δ_2 such that, for any state space realization of $G(s)$,

$$|x(t)| < \delta_1 [|x(0)| + \delta_2] \quad \forall t \geq 0$$

FOR ALL P-class nonlinearities

CT Asymptotic Hyperstability

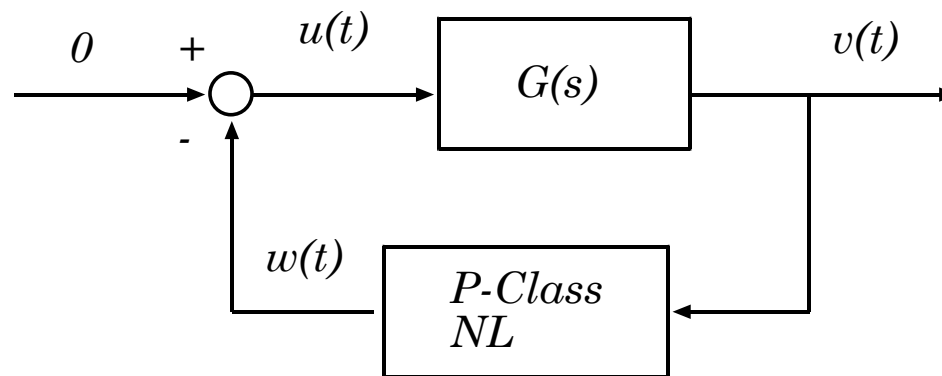


Asymptotic Hyperstability: The above feedback system is asymptotically hyperstable if

1. It is hyperstable
2. For all signals $|w(t)| < \infty$ (I.e. bounded output of any P-class nonlinearity), and any state space realization of $G(s)$,

$$\lim_{t \rightarrow \infty} x(t) = 0$$

CT Hyperstability Theorems



Hyperstability Theorem: The above feedback system is hyperstable **iff** the transfer function $G(s)$ of the LTI block is **Positive Real**.

Asymptotical Hyperstability Theorem: The above feedback system is asymptotically hyperstable **iff** the transfer function $G(s)$ of the LTI block is **Strictly Positive Real**.

CT Positive Real TF

$$G(s) = C(sI - A)^{-1}B + D$$

Is **Positive Real** iff:

1. $G(s)$ does not have any unstable poles (I.e. no $\text{Re}\{s\} > 0$).
2. Any pole of $G(s)$ that is in the imaginary axis does not repeat and its associated residue (I.e. the coefficient appearing in the partial fraction expansion) is non-negative.
3. $2 \text{Re}\{G(j\omega)\} = G(j\omega) + G^T(-j\omega) \geq 0$

for all real ω 's for which $s = j\omega$ is not a pole of $G(s)$

Strictly Positive Real (SPR) TF

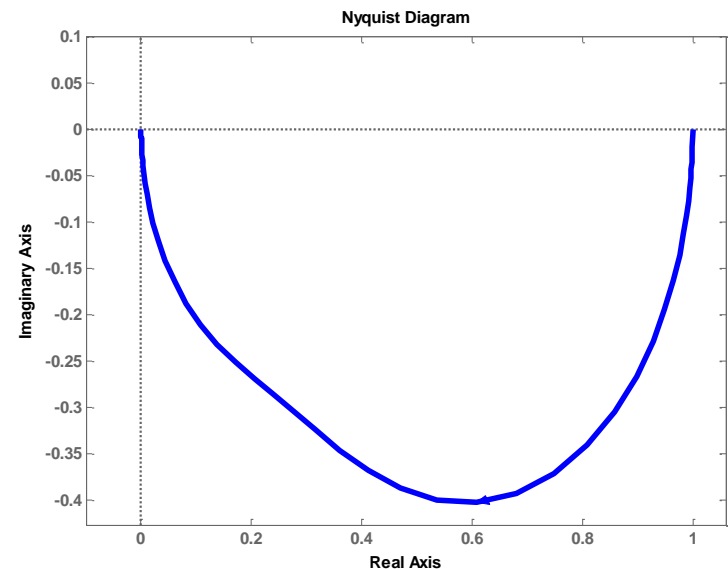
$$G(s) = C(sI - A)^{-1}B + D$$

Is **Strictly Positive Real (SPR)** iff:

1. All poles of $G(s)$ are asymptotically stable.
2. $2 \operatorname{Re}\{G(j\omega)\} = G(j\omega) + G^T(-j\omega) > 0$
for all ω , $0 \leq \omega < \infty$

Example:

$$G(s) = \frac{s + 1}{s^2 + 3s + 1}$$



Strictly Positive Real (SPR) TF

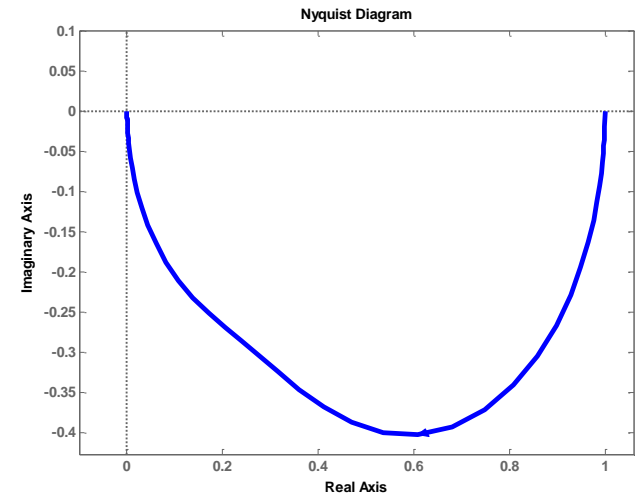
For scalar rational transfer functions

$$G(s) = \frac{B(s)}{A(s)}$$

1. All poles of $G(s)$ are asymptotically stable.
2. $\operatorname{Re}\{G(j\omega)\} > 0$ for all ω , $0 \leq \omega < \infty$

Note:

A necessary (but not sufficient) condition for $G(s)$ to be SPR is that its relative degree must be less than or equal to 1.



Kalman Yakubovich Popov Lemma

$$G(s) = C(sI - A)^{-1}B + D$$

Is **Strictly Positive Real (SPR)** if and only if

- there exist a symmetric and positive definite matrix P ,
- matrices L and K ,
- and a constant $\epsilon > 0$ such that

$$A^T P + P A = -L^T L - \epsilon P$$

$$B^T P - C = -K^T L$$

$$D + D^T = K^T K$$

Kalman Yakubovich Popov Lemma

$$G(s) = C(sI - A)^{-1}B$$

Is **Strictly Positive Real (SPR)** iff there exist symmetric and positive definite matrices P and Q , such that:

$$A^T P + P A = -Q$$

$$B^T P = C$$

SPR TF implies Positivity

Let $G(s) = C(sI - A)^{-1}B + D$ be SPR

Then there exist positive definite functions

$$V(x) \succ 0 \quad \lambda_1(x) \succ 0$$

and a positive semi-definite function $\lambda_2(x, u) \succeq 0$

Such that the input $u(t)$ output $y(t)$ pair satisfies

$$\begin{aligned} \int_0^t y^T u \, d\tau &= V(x(t)) - V(x(0)) + \int_0^t (\lambda_1(x) + \lambda_2(x, u)) \, d\tau \\ &\geq -\gamma_o^2 \end{aligned}$$

$$\gamma_o^2 = V(x(0))$$

SPR TF implies Passivity

Proof: We consider a strictly causal transfer function

$$G(s) = C(sI - A)^{-1}B$$

which is SPR, with state space realization

$$\begin{aligned}\frac{d}{dt}x &= Ax + Bu \\ v &= Cx\end{aligned}$$

By the Kalman Yakubovich, Popov lemma, there exist symmetric and positive definite matrices P and Q , such that

$$\begin{aligned}A^T P + PA &= -Q \\ B^T P &= C\end{aligned}$$

SPR TF implies Passivity

Proof: Thus, since $v = Cx$

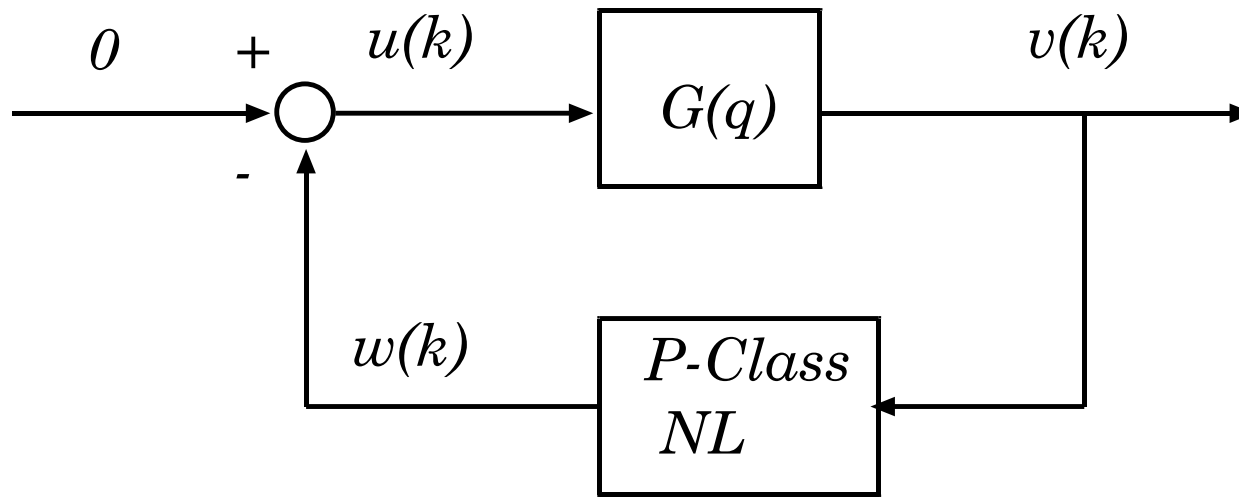
$$u^T v = \dot{V} + \frac{1}{2}x^T Qx$$

Define the PD function $\lambda_1(x) = \frac{1}{2}x^T Qx$ and integrate

$$\begin{aligned} \int_0^t u^T v d\tau &= \int_0^t \dot{V} d\tau + \int_0^t \lambda_1(x) d\tau \\ &= V(x(t)) - V(x(0)) + \int_0^t \lambda_1(x) d\tau \end{aligned}$$

DT Hyperstability Theory

$$G(z) = C(zI - A)^{-1}B + D$$

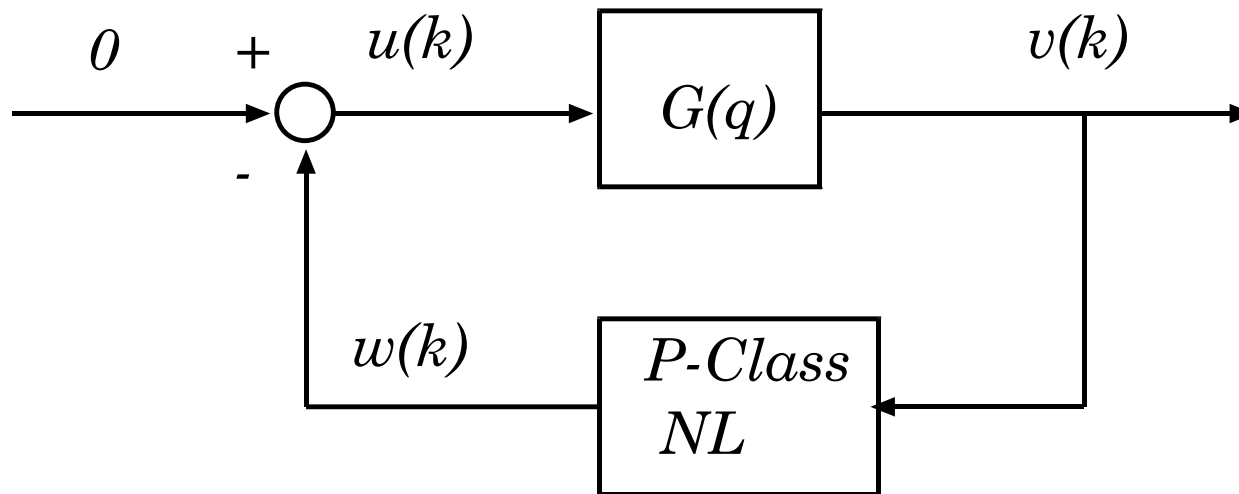


- State space description of the LTI Block:

$$x(k + 1) = Ax(k) + Bu(k)$$

$$v(k) = Cx(k) + Du(k)$$

DT Hyperstability Theory

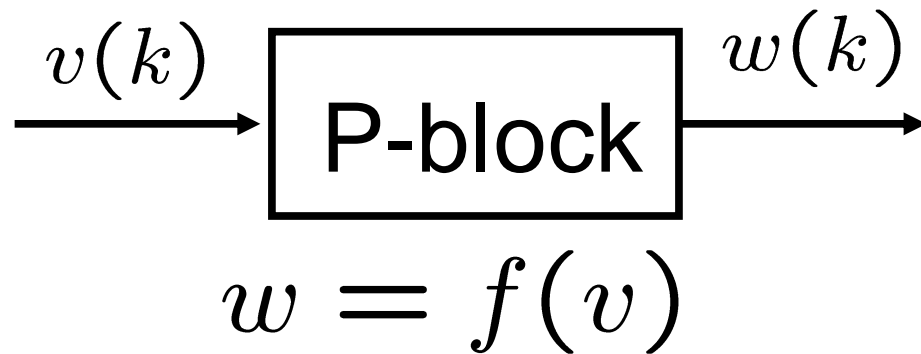


- P-class nonlinearity: (passive nonlinearities)

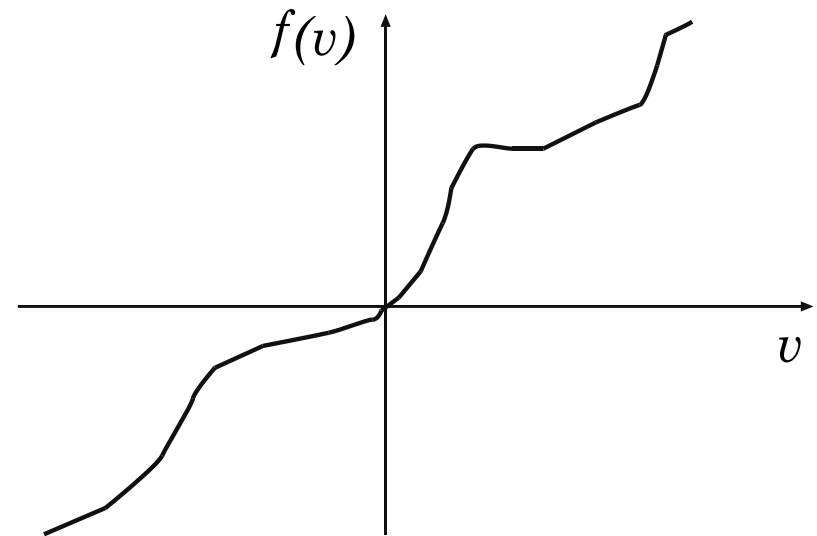
$$\sum_{j=0}^k w^T(j)v(j) \geq -\gamma_0^2 \quad \forall k \geq 0$$

Where γ_0 is a bounded constant.

Example: Static nonlinearity:

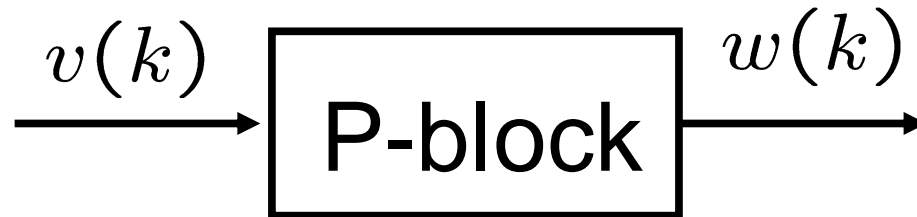


$$v f(v) \geq 0$$



$$\sum_{j=0}^k w^T(j)v(j) = \sum_{j=0}^k \underbrace{f(v(j))v(j)}_{\geq 0} \geq 0 > -\gamma_0^2$$

Example: Dynamic P-class block



$$\left\{ \begin{array}{l} \tilde{\theta}(k) = \tilde{\theta}(k-1) + F \phi(k)v(k) \\ w(k) = \phi^T(k)\tilde{\theta}(k) \end{array} \right. \quad \begin{array}{l} \phi(k) \in \mathcal{R}^n \\ \tilde{\theta}(-1) \in \mathcal{R}^n \end{array}$$

$$F = F^T \succ 0$$

$$\|\tilde{\theta}(-1)\| < \infty$$

$$\|\phi(k)\| < \infty$$

Example: Dynamic P-class block

$$w(k) = \phi^T(k)\tilde{\theta}(k) \quad \tilde{\theta}(k) = \tilde{\theta}(k-1) + F\phi(k)v(k)$$

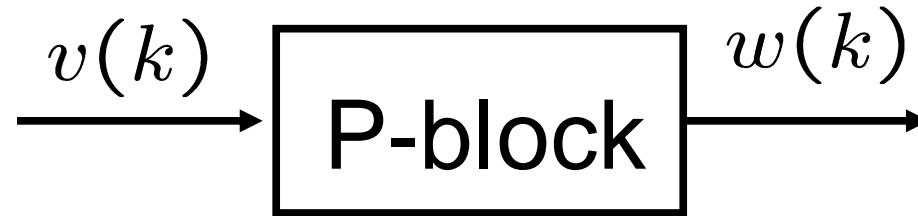
$$\begin{aligned} \sum_{j=0}^k w(j)v(j) &= \sum_{j=0}^k \phi^T(j)\tilde{\theta}(j)v(j) \\ &= \sum_{j=0}^k \tilde{\theta}^T(j) \underbrace{[\phi(j)v(j)]}_{F^{-1}[\tilde{\theta}(j) - \tilde{\theta}(j-1)]} \\ &= \sum_{j=0}^k \tilde{\theta}^T(j) F^{-1} [\tilde{\theta}(j) - \tilde{\theta}(j-1)] \\ &= \sum_{j=0}^k \left\{ \tilde{\theta}^T(j) F^{-1} \tilde{\theta}(j) - \tilde{\theta}^T(j) F^{-1} \tilde{\theta}(j-1) \right\} \end{aligned}$$

Example: Dynamic P-class block

$$\begin{aligned} \sum_{j=0}^k w(j)v(j) &= \sum_{j=0}^k \left\{ \tilde{\theta}^T(j)F^{-1}\tilde{\theta}(j) - \tilde{\theta}^T(j)F^{-1}\tilde{\theta}(j-1) \right\} \\ &+ \frac{1}{2} \sum_{j=0}^k \tilde{\theta}^T(j-1)F^{-1}\tilde{\theta}(j-1) - \frac{1}{2} \sum_{j=0}^k \tilde{\theta}^T(j-1)F^{-1}\tilde{\theta}(j-1) \end{aligned}$$

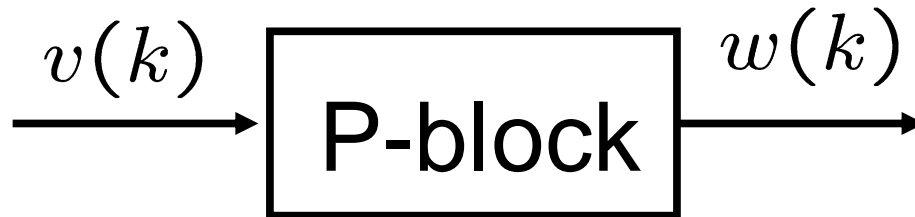
$$\begin{aligned} \sum_{j=0}^k w(j)v(j) &= \frac{1}{2} \sum_{j=0}^k \left\{ \tilde{\theta}^T(j)F^{-1}\tilde{\theta}(j) - \tilde{\theta}^T(j-1)F^{-1}\tilde{\theta}(j-1) \right\} \\ &+ \underbrace{\frac{1}{2} \sum_{j=0}^k \left[\tilde{\theta}(j) - \tilde{\theta}(j-1) \right]^T F^{-1} \left[\tilde{\theta}(j) - \tilde{\theta}(j-1) \right]}_{\geq 0} \end{aligned}$$

Example: Dynamic P-class block



$$\begin{aligned}
 \sum_{j=0}^k w(j)v(j) &\geq \frac{1}{2} \sum_{j=0}^k \left\{ \tilde{\theta}^T(j) F^{-1} \tilde{\theta}(j) - \tilde{\theta}^T(j-1) F^{-1} \tilde{\theta}(j-1) \right\} \\
 &= \frac{1}{2} \tilde{\theta}^T(k) F^{-1} \tilde{\theta}(k) - \underbrace{\frac{1}{2} \tilde{\theta}^T(-1) F^{-1} \tilde{\theta}(-1)}_{\gamma_o^2} \\
 &\geq -\gamma_o^2
 \end{aligned}$$

Example: Dynamic P-class block



$$\left\{ \begin{array}{l} \tilde{\theta}(k) = \tilde{\theta}(k-1) + F\phi(k-1)v(k) \\ w(k) = \phi^T(k-1)\tilde{\theta}(k) \end{array} \right. \quad \begin{array}{l} \phi(k) \in \mathcal{R}^n \\ \tilde{\theta}(-1) \in \mathcal{R}^n \end{array}$$

$$F = F^T \succ 0$$

$$\|\tilde{\theta}(-1)\| < \infty$$

$$\|\phi(k)\| < \infty$$

Example: Dynamic P-class block

$$w(k) = \phi^T(k-1)\tilde{\theta}(k) \quad \tilde{\theta}(k) = \tilde{\theta}(k-1) + F\phi(k-1)v(k)$$

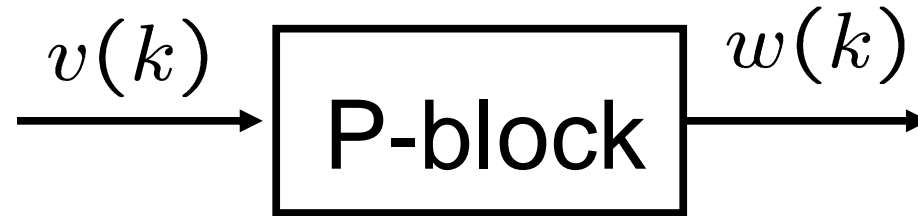
$$\begin{aligned} \sum_{j=0}^k w(j)v(j) &= \sum_{j=0}^k \phi^T(j-1)\tilde{\theta}(j)v(j) \\ &= \sum_{j=0}^k \tilde{\theta}^T(j) \underbrace{[\phi(j-1)v(j)]}_{F^{-1}[\tilde{\theta}(j) - \tilde{\theta}(j-1)]} \\ &= \sum_{j=0}^k \tilde{\theta}^T(j) F^{-1} [\tilde{\theta}(j) - \tilde{\theta}(j-1)] \\ &= \sum_{j=0}^k \left\{ \tilde{\theta}^T(j) F^{-1} \tilde{\theta}(j) - \tilde{\theta}^T(j) F^{-1} \tilde{\theta}(j-1) \right\} \end{aligned}$$

Example: Dynamic P-class block

$$\begin{aligned} \sum_{j=0}^k w(j)v(j) &= \sum_{j=0}^k \left\{ \tilde{\theta}^T(j)F^{-1}\tilde{\theta}(j) - \tilde{\theta}^T(j)F^{-1}\tilde{\theta}(j-1) \right\} \\ &+ \frac{1}{2} \sum_{j=0}^k \tilde{\theta}^T(j-1)F^{-1}\tilde{\theta}(j-1) - \frac{1}{2} \sum_{j=0}^k \tilde{\theta}^T(j-1)F^{-1}\tilde{\theta}(j-1) \end{aligned}$$

$$\begin{aligned} \sum_{j=0}^k w(j)v(j) &= \frac{1}{2} \sum_{j=0}^k \left\{ \tilde{\theta}^T(j)F^{-1}\tilde{\theta}(j) - \tilde{\theta}^T(j-1)F^{-1}\tilde{\theta}(j-1) \right\} \\ &+ \underbrace{\frac{1}{2} \sum_{j=0}^k \left[\tilde{\theta}(j) - \tilde{\theta}(j-1) \right]^T F^{-1} \left[\tilde{\theta}(j) - \tilde{\theta}(j-1) \right]}_{\geq 0} \end{aligned}$$

Example: Dynamic P-class block

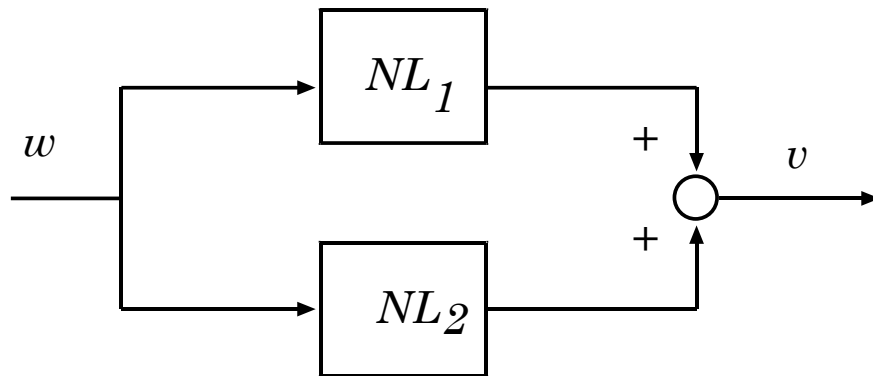


$$\begin{aligned}
 \sum_{j=0}^k w(j)v(j) &\geq \frac{1}{2} \sum_{j=0}^k \left\{ \tilde{\theta}^T(j) F^{-1} \tilde{\theta}(j) - \tilde{\theta}^T(j-1) F^{-1} \tilde{\theta}(j-1) \right\} \\
 &= \frac{1}{2} \tilde{\theta}^T(k) F^{-1} \tilde{\theta}(k) - \underbrace{\frac{1}{2} \tilde{\theta}^T(-1) F^{-1} \tilde{\theta}(-1)}_{\gamma_o^2} \\
 &\geq -\gamma_o^2
 \end{aligned}$$

Examples of P-class NL

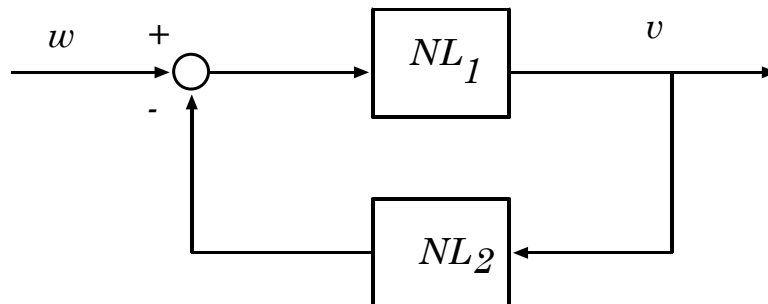
Lemma:

- The parallel combination of two P-class nonlinearities is also a P-class nonlinearity.



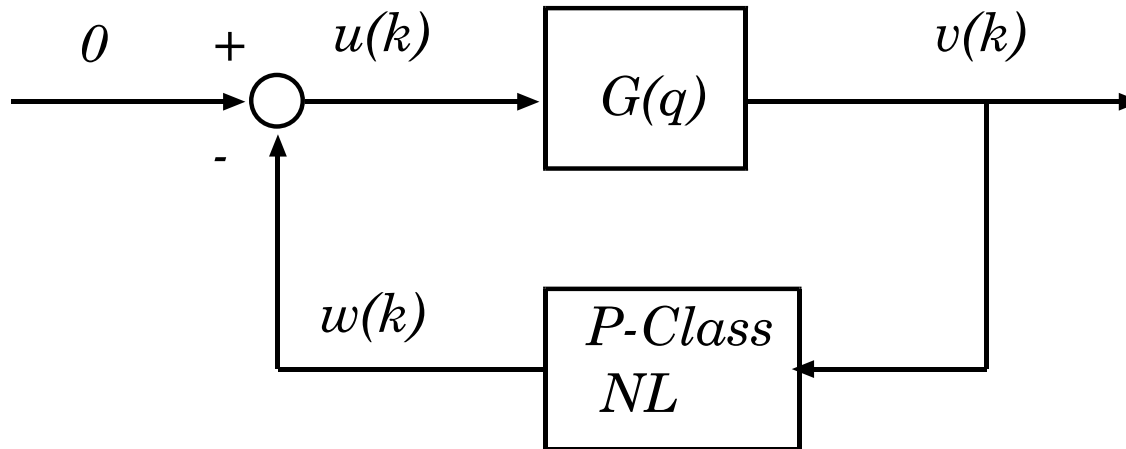
$$\sum_{j=0}^k w^T(j)v(j) \geq -\gamma_o^2$$

- The feedback combination of two P-class nonlinearities is also a P-class nonlinearity.



$$\sum_{j=0}^k w^T(j)v(j) \geq -\gamma_o^2$$

DT Hyperstability

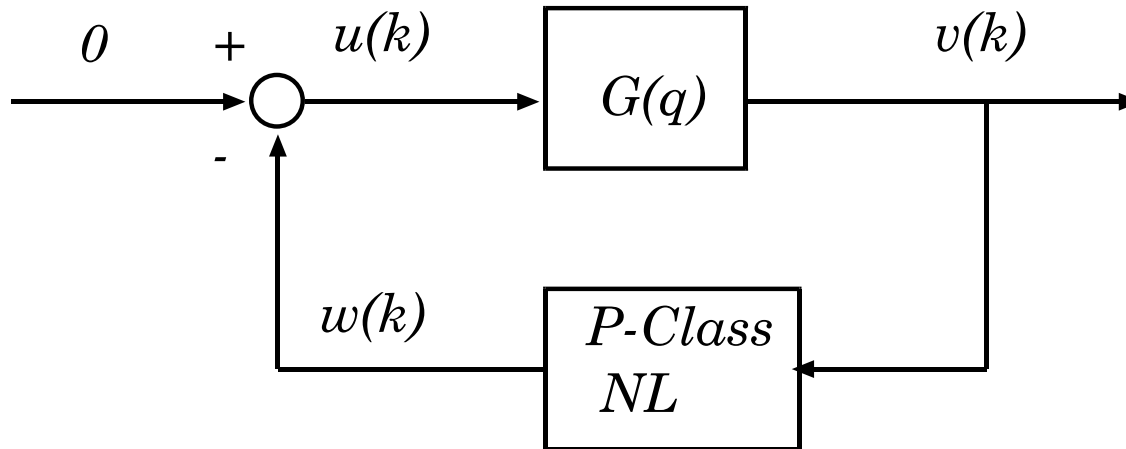


Hyperstability: The above feedback system is hyperstable if there exist positive bounded constants δ_1, δ_2 such that, for any state space realization of $G(q)$,

$$\|x(k)\| < \delta_1 [\|x(0)\| + \delta_2] \quad \forall k \geq 0$$

FOR ALL P-class nonlinearities

DT Asymptotic Hyperstability

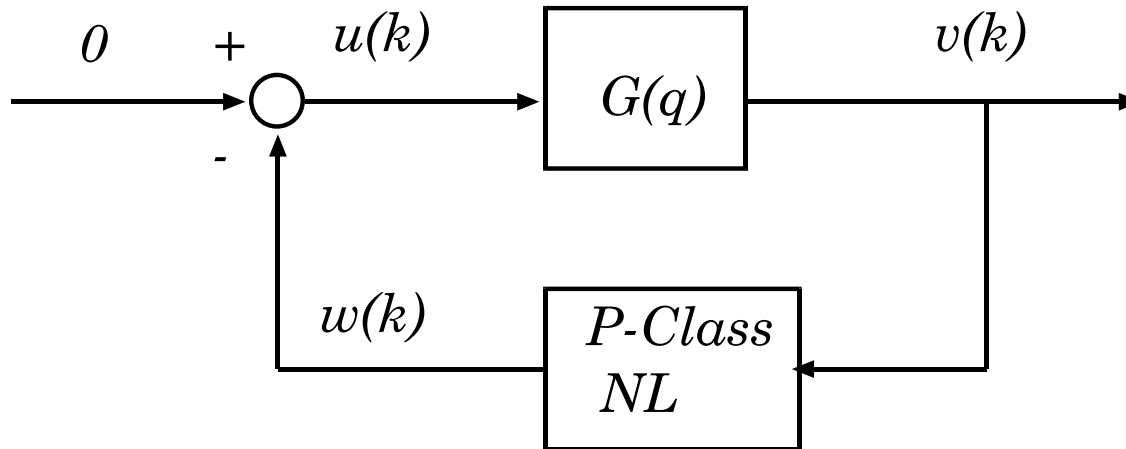


Asymptotic Hyperstability: The above feedback system is asymptotically hyperstable if

1. It is hyperstable
2. for any state space realization of $G(z)$,

$$\lim_{k \rightarrow \infty} x(k) = 0$$

DT Hyperstability Theorems



Hyperstability Theorem: The above feedback system is hyperstable **iff** the transfer function $G(z)$ of the LTI block is **Positive Real**.

Asymptotical Hyperstability Theorem: The above feedback system is asymptotically hyperstable **iff** the transfer function $G(z)$ of the LTI block is **Strictly Positive Real**.

Positive Real TF

$$G(z) = C(zI - A)^{-1}B + D$$

Is **Positive Real** iff:

1. $G(z)$ does not have any unstable poles (i.e. no $|z| > 1$).
2. Any pole of $G(z)$ that is in the unit circle does not repeat and its associated residue (i.e. the coefficient appearing in the partial fraction expansion) is non-negative.
3. $G(e^{j\omega}) + G^T(e^{-j\omega}) \succeq 0$

for all $\omega \in [0, \pi]$ for which $z = e^{j\omega}$ is not a pole of $G(z)$

Strictly Positive Real (SPR) TF

$$G(z) = C(zI - A)^{-1}B + D$$

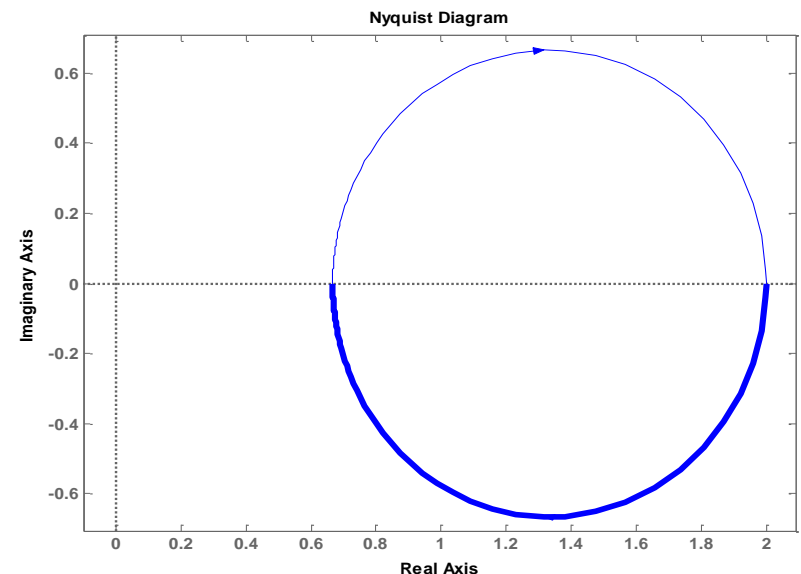
Is **Strictly Positive Real (SPR)** iff:

1. All poles of $G(z)$ are asymptotically stable.
2. $G(e^{j\omega}) + G^T(e^{-j\omega}) \succ 0$

for all $0 \leq \omega \leq \pi$

Example:

$$G(z) = \frac{z}{z + 0.5}$$



Strictly Positive Real (SPR) TF

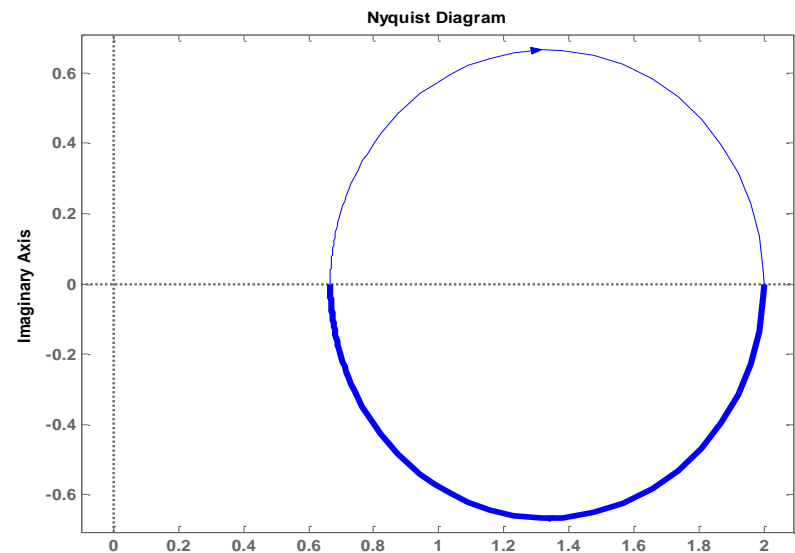
For scalar rational transfer functions

$$G(z) = \frac{B(z)}{A(z)}$$

1. All poles of $G(z)$ are asymptotically stable.
2. $\text{Re}\{G(e^{j\omega})\} > 0$ for all ω , $0 \leq \omega \leq \pi$

Note:

A necessary (but not sufficient) condition for $G(z)$ to be SPR is that its relative degree must be 0.



Matrix Inequality Interpretation of SPR

The transfer function

$$G(z) = C(zI - A)^{-1}B + D$$

is **Strictly Positive Real (SPR)** if and only if

there exists $P \succ 0$ such that

$$\begin{bmatrix} A^T P A - P & A^T P B - C^T \\ B^T P A - C & B^T P B - D - D^T \end{bmatrix} \prec 0$$

SPR state-space realization fact

Theorem: If $G(z) = C(zI-A)^{-1}B + D$ is SPR, then

$$D + D^T \succ 0$$

Proof: Choose $P \succ 0$ such that

$$\begin{bmatrix} A^T P A - P & A^T P B - C^T \\ B^T P A - C & B^T P B - D - D^T \end{bmatrix} \prec 0$$

Note that

$$B^T P B - D - D^T \prec 0$$

$$\Rightarrow D + D^T \succ B^T P B \succeq 0$$



SPR TF is P-class

Let $G(z) = C(zI - A)^{-1}B + D$ be SPR

Then there exist positive definite functions

$$V(x) \succ 0 \quad \lambda_1(x, u) \succ 0$$

Such that any input $u(k)$ output $y(k)$ pair satisfies

$$\sum_{j=0}^k y^T(j)u(j) = V(x(k+1)) - V(x(0)) + \sum_{j=0}^k \lambda_1(x(j), u(j))$$

$$\geq -\gamma_0^2 \quad \gamma_0^2 = V(x(0))$$

Shorthand notation

$$x(k) \rightarrow x_k$$

$$u(k) \rightarrow u_k$$

$$y(k) \rightarrow y_k$$

$$v(k) \rightarrow v_k$$

$$w(k) \rightarrow w_k$$

Proof

Let $G(z) = C(zI - A)^{-1}B + D$ be SPR

Choose $P \succ 0$ such that

$$\begin{bmatrix} A^T P A - P & A^T P B - C^T \\ B^T P A - C & B^T P B - D - D^T \end{bmatrix} \prec 0$$

Define the Lyapunov function

$$V(x_k) = \frac{1}{2} x_k^T P x_k \succ 0$$

and the function

$$\lambda_1(x, u) = -\frac{1}{2} \begin{bmatrix} x \\ u \end{bmatrix}^T \begin{bmatrix} A^T P A - P & A^T P B - C^T \\ B^T P A - C & B^T P B - D - D^T \end{bmatrix} \begin{bmatrix} x \\ u \end{bmatrix} \succ 0$$

Proof

$$\begin{aligned}
 V(x_{k+1}) - V(x_k) &= \frac{1}{2}(Ax_k + Bu_k)^T P(Ax_k + Bu_k) - \frac{1}{2}x_k^T P x_k \\
 &= \frac{1}{2} \begin{bmatrix} x_k \\ u_k \end{bmatrix}^T \begin{bmatrix} A^T P A - P & A^T P B \\ B^T P A & B^T P B \end{bmatrix} \begin{bmatrix} x_k \\ u_k \end{bmatrix} \\
 &= \frac{1}{2} \begin{bmatrix} x_k \\ u_k \end{bmatrix}^T \begin{bmatrix} A^T P A - P & A^T P B - C^T \\ B^T P A - C & B^T P B - D - D^T \end{bmatrix} \begin{bmatrix} x_k \\ u_k \end{bmatrix} \\
 &\quad + \frac{1}{2} [u_k^T C x_k + u_k^T D u_k + u_k^T D^T u_k + x_k^T C^T u_k] \\
 &= -\lambda_1(x_k, u_k) + (C x_k + D u_k)^T u_k \\
 &= -\lambda_1(x_k, u_k) + y_k^T u_k
 \end{aligned}$$

Proof

From the previous slide

$$V(x_{k+1}) - V(x_k) = -\lambda_1(x_k, u_k) + y_k^T u_k$$

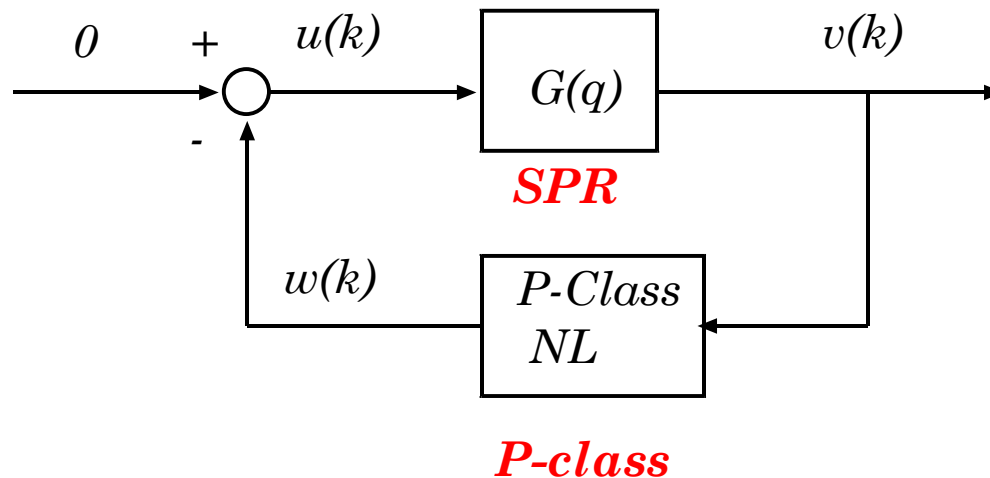
$$\Rightarrow y_k^T u_k = V(x_{k+1}) - V(x_k) + \lambda_1(x_k, u_k)$$

Summing both sides of the equation yields

$$\sum_{j=0}^k y_j^T u_j = V(x_{k+1}) - V(x_0) + \sum_{j=0}^k \lambda_1(x_j, u_j)$$

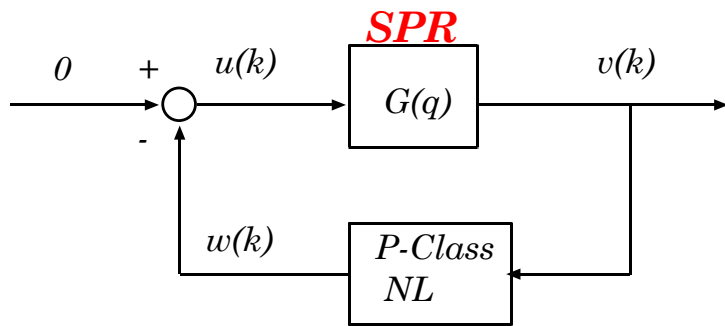


Proof of the sufficiency part of the Asymptotic Hyperstability Theorem - Discrete Time



- Since the nonlinearity is P-class, $\sum_{j=0}^k w_j^T v_j \geq -\gamma_1^2$
- Since LTI block is SPR, we can use the choose $P \succ 0$ such that

$$\begin{bmatrix} A^T P A - P & A^T P B - C^T \\ B^T P A - C & B^T P B - D - D^T \end{bmatrix} \prec 0$$



Hyperstability

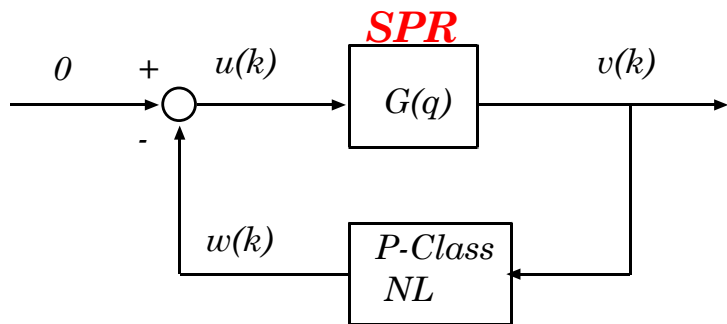
From the previous proof (SPR TF is P-class), we have

$$\sum_{j=0}^k v_j^T u_j = V(x_{k+1}) - V(x_0) + \sum_{j=0}^k \lambda_1(x_j, u_j)$$

where

$$V(x_k) = \frac{1}{2} x_k^T P x_k \succ 0$$

$$\lambda_1(x, u) = -\frac{1}{2} \begin{bmatrix} x \\ u \end{bmatrix}^T \begin{bmatrix} A^T P A - P & A^T P B - C^T \\ B^T P A - C & B^T P B - D - D^T \end{bmatrix} \begin{bmatrix} x \\ u \end{bmatrix} \succ 0$$



Hyperstability

$$G(z) = C(zI - A)^{-1}B + D$$

Rearranging terms,

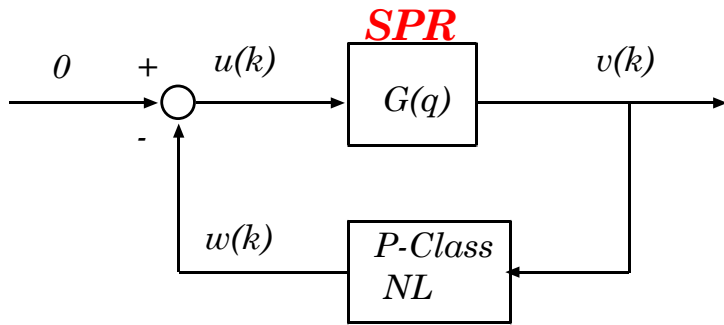
$$V(x_{k+1}) = V(x_0) + \sum_{j=0}^k v_j^T u_j - \sum_{j=0}^k \lambda_1(x_j, u_j)$$

From the P-class nonlinearity:

$$\sum_{j=0}^k w_j^T v_j \geq -\gamma_1^2 \quad \rightarrow \quad \sum_{j=0}^k v_j^T u_j \leq \gamma_1^2$$

Therefore,

$$V(x_{k+1}) \leq V(x_0) + \gamma_1^2 - \underbrace{\sum_{j=0}^k \lambda_1(x_j, u_j)}_{\geq 0} \leq V(x_0) + \gamma_1^2$$



Hyperstability

$$G(z) = C(zI - A)^{-1}B + D$$

From the previous slide

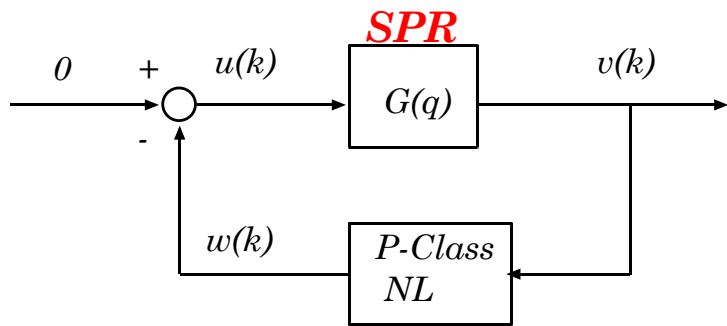
$$V(x_k) \leq V(x_0) + \gamma_1^2$$

$$\Rightarrow \frac{1}{2}x_k^T P x_k \leq \frac{1}{2}x_0^T P x_0 + \gamma_1^2$$

$$\Rightarrow \lambda_{\min}(P)\|x_k\|^2 \leq \lambda_{\max}(P)\|x_0\|^2 + 2\gamma_1^2$$

$$\Rightarrow \|x_k\|^2 \leq \frac{\lambda_{\max}(P)}{\lambda_{\min}(P)} \left(\|x_0\|^2 + \frac{2}{\lambda_{\max}(P)} \gamma_1^2 \right)$$

Therefore, the feedback system is hyperstable



Asymptotic Hyperstability

$$G(z) = C(zI - A)^{-1}B + D$$

$$0 \leq V(x_{k+1}) \leq V(x_0) + \gamma_1^2 - \sum_{j=0}^k \lambda_1(x_j, u_j)$$

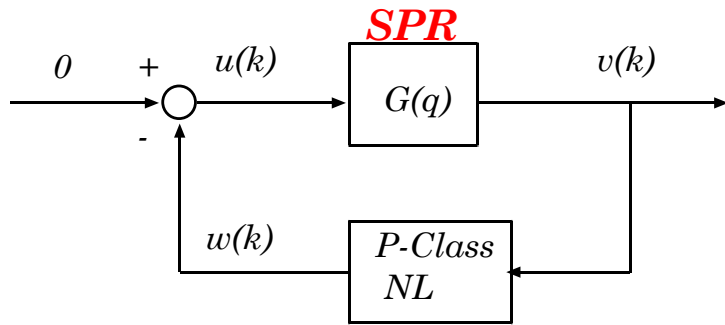
$$\Rightarrow \underbrace{\sum_{j=0}^k \lambda_1(x_j, u_j)}_{\leftarrow} \leq V(x_0) + \gamma_1^2$$

- monotonic nondecreasing sequence in k
- bounded above

$$\Rightarrow \lim_{k \rightarrow \infty} \lambda_1(x_k, u_k) = 0 \quad \Rightarrow \quad \lim_{k \rightarrow \infty} x_k = 0, \quad \lim_{k \rightarrow \infty} u_k = 0$$

Therefore, the feedback system is asymptotically hyperstable





Additional Result

$$G(z) = C(zI - A)^{-1}B + D$$

We have already shown that

$$\lim_{k \rightarrow \infty} x_k = 0,$$

$$\lim_{k \rightarrow \infty} u_k = 0$$

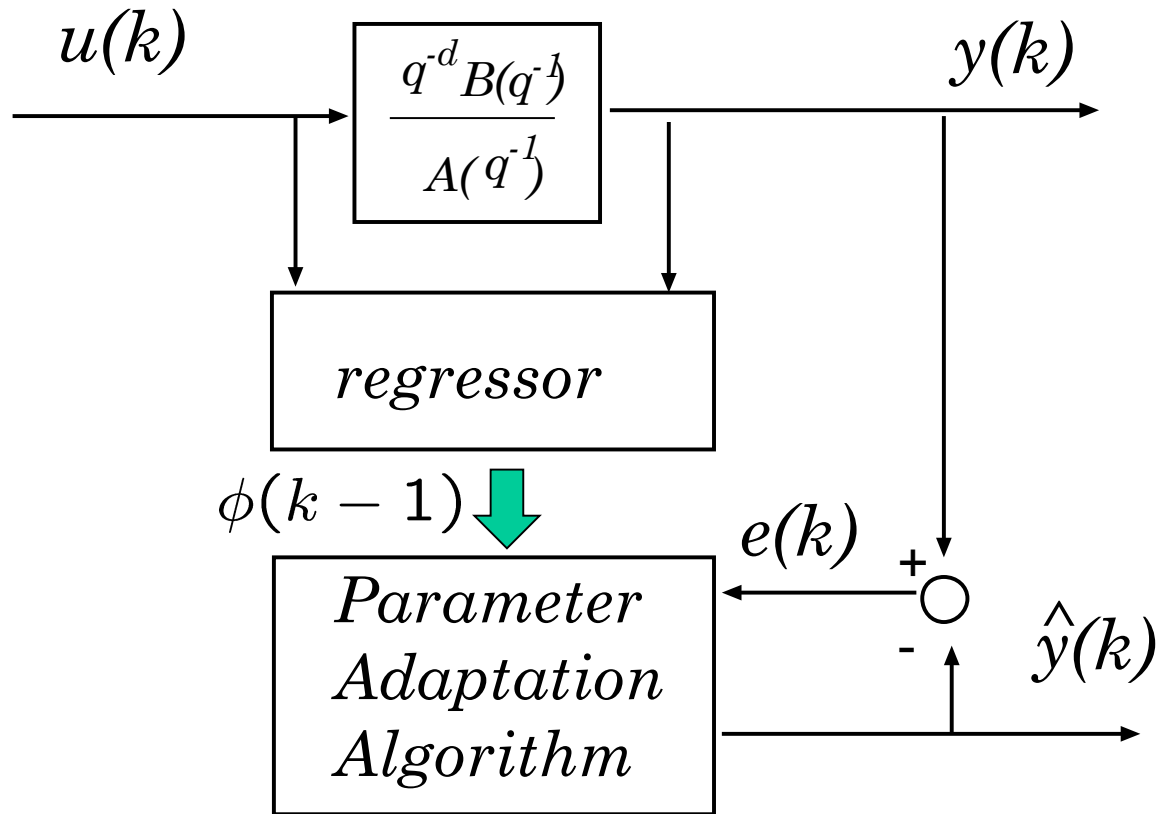
From this we see that

$$\lim_{k \rightarrow \infty} v_k = \lim_{k \rightarrow \infty} (Cx_k + Du_k) = 0$$

$$\lim_{k \rightarrow \infty} w_k = \lim_{k \rightarrow \infty} (-u_k) = 0$$

Therefore, $x(k)$, $u(k)$, $v(k)$, and $w(k)$ converge to 0

Stability analysis of Series-parallel ID



Series-Parallel ID Dynamics (review)

a-posteriori error:

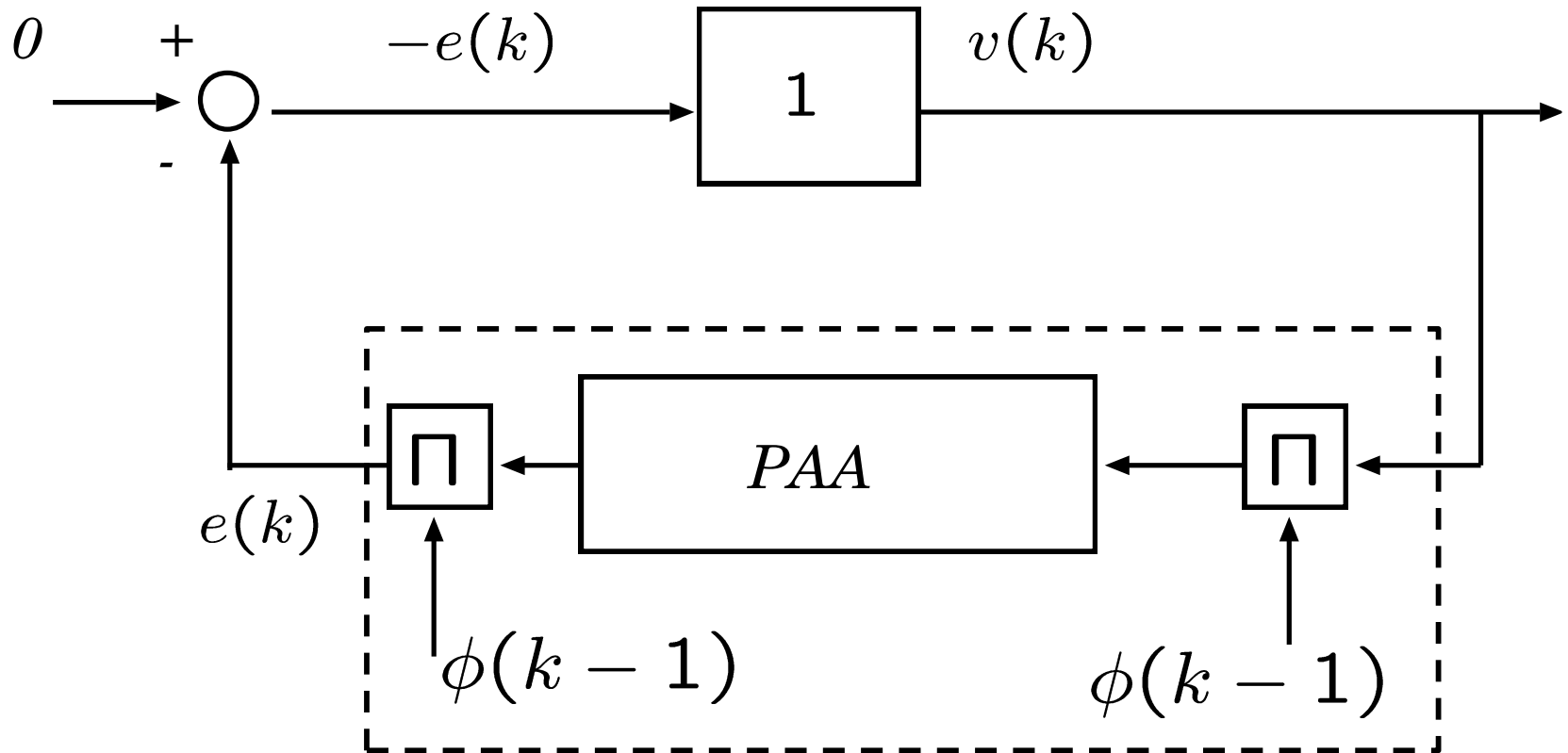
$$e(k) = y(k) - \hat{y}(k)$$

$$e(k) = \phi^T(k-1)\tilde{\theta}(k)$$

Parameter error update law: $\tilde{\theta}(k) = \theta - \hat{\theta}(k)$

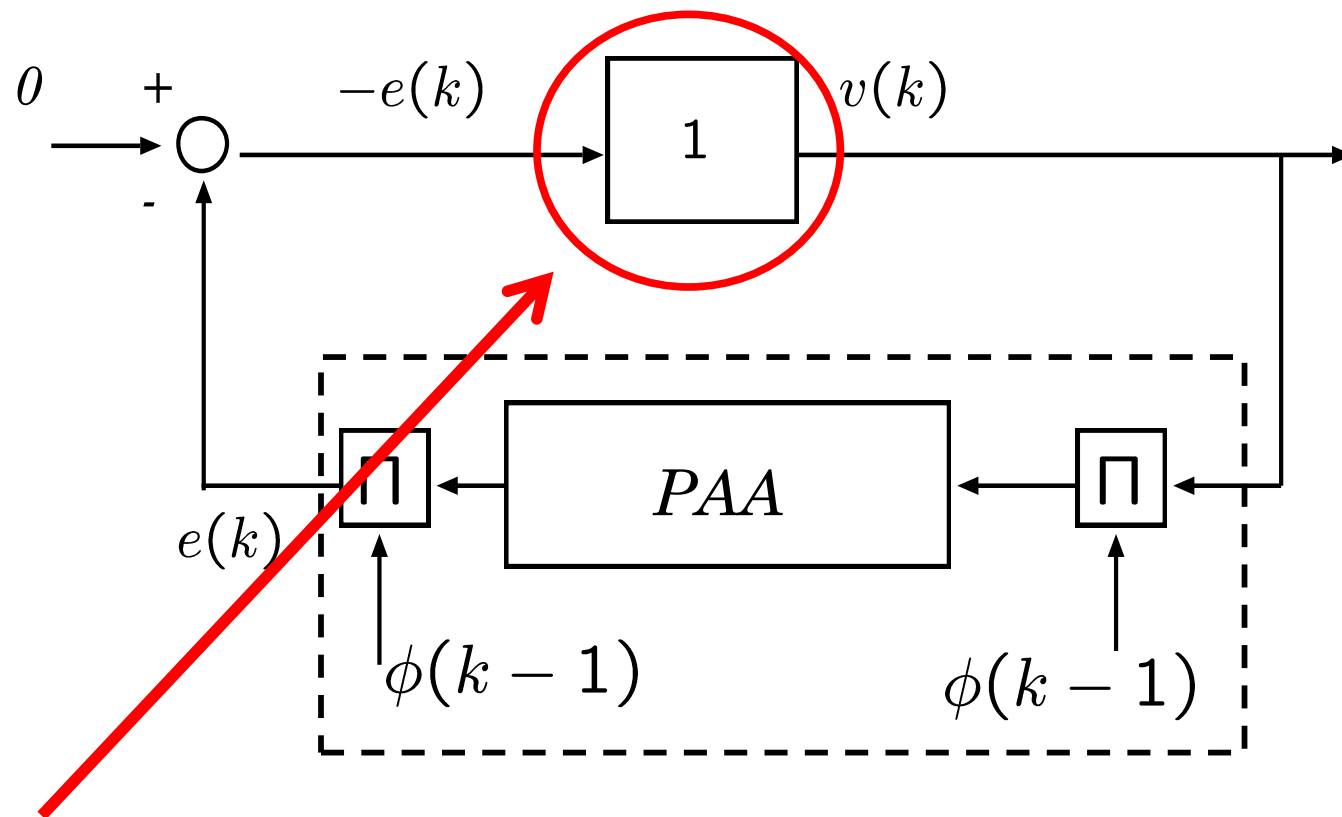
$$\tilde{\theta}(k) = \tilde{\theta}(k-1) - F \phi(k-1)e(k)$$

Series-Parallel ID Dynamics (review)



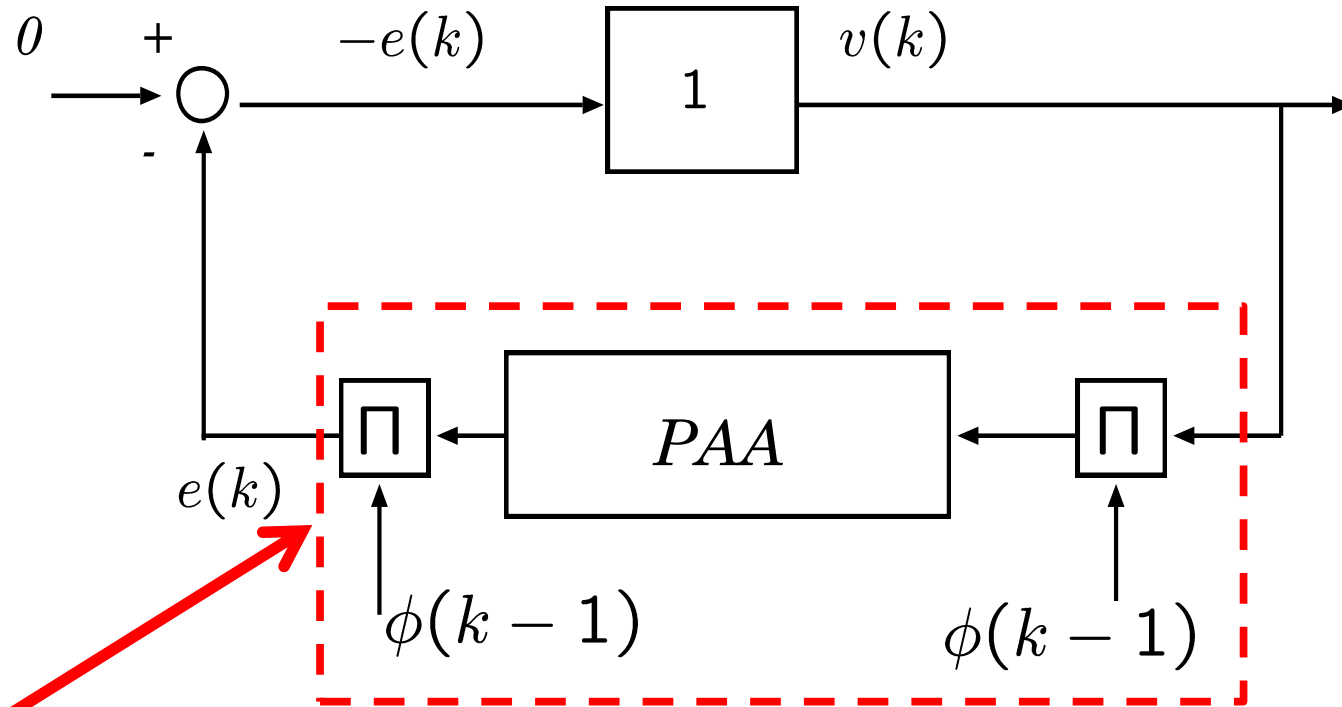
$PAA:$
$$\tilde{\theta}(k) = \tilde{\theta}(k-1) + F \phi(k-1)v(k)$$

Stability analysis of Series-parallel ID



Strictly Positive Real

Stability analysis of Series-parallel ID



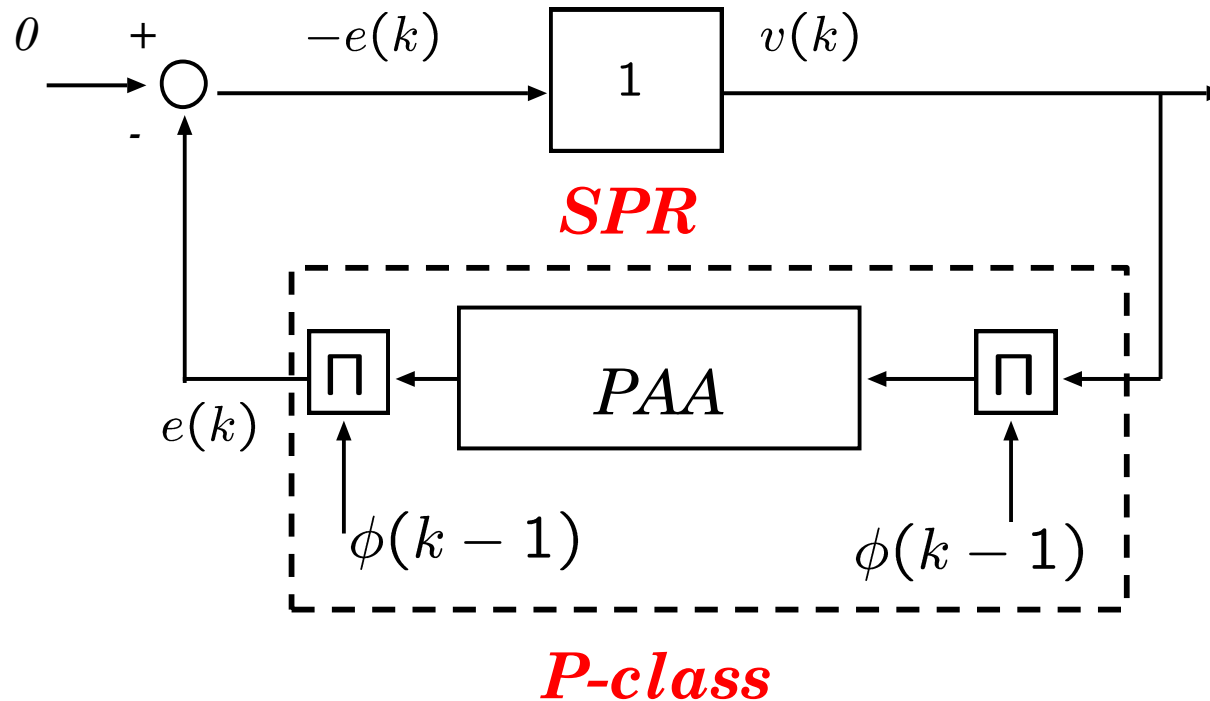
$$\tilde{\theta}(k) = \tilde{\theta}(k-1) + F \phi(k-1)v(k)$$

$$e(k) = \phi^T(k-1)\tilde{\theta}(k)$$



$$\sum_{j=0}^k e^T(j)v(j) \geq -\gamma_o^2$$

Stability analysis of Series-parallel ID

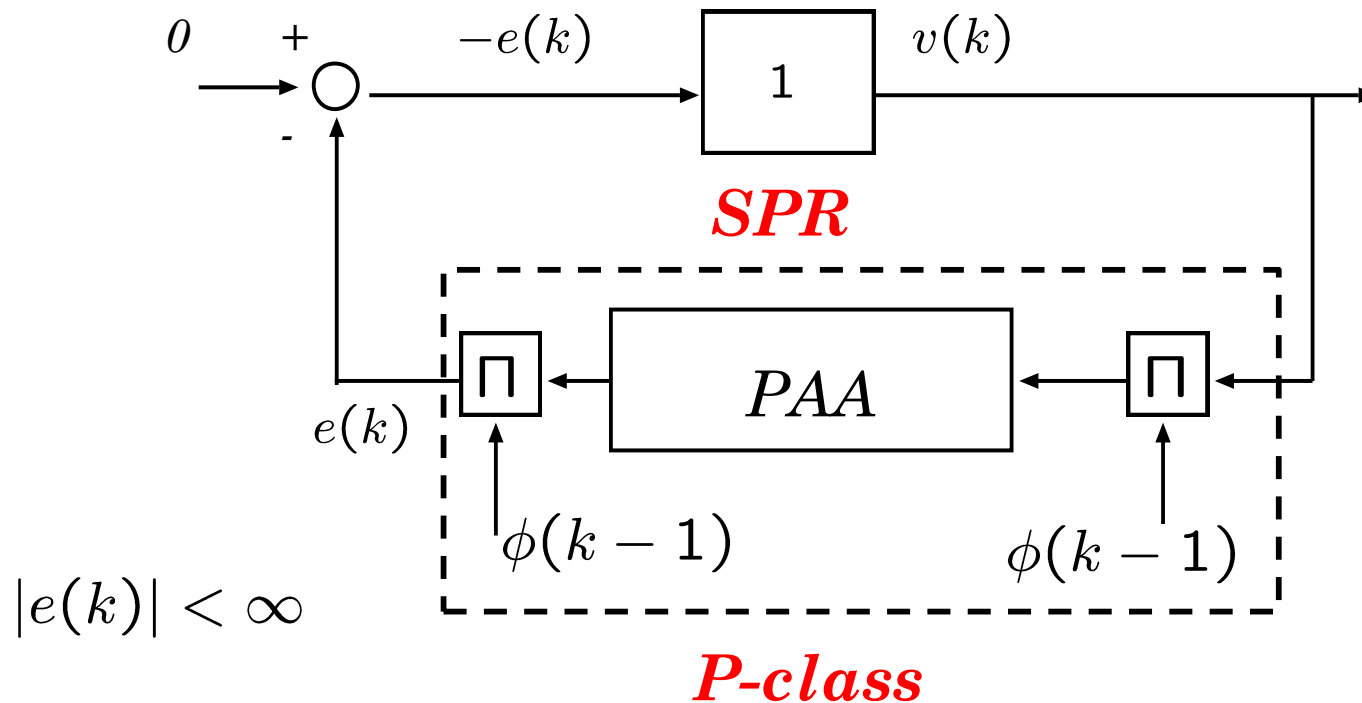


By the sufficiency portion of Hyperstability Theorem:

$$|v(k)| < \infty$$

$$|e(k)| < \infty$$

Stability analysis of Series-parallel ID



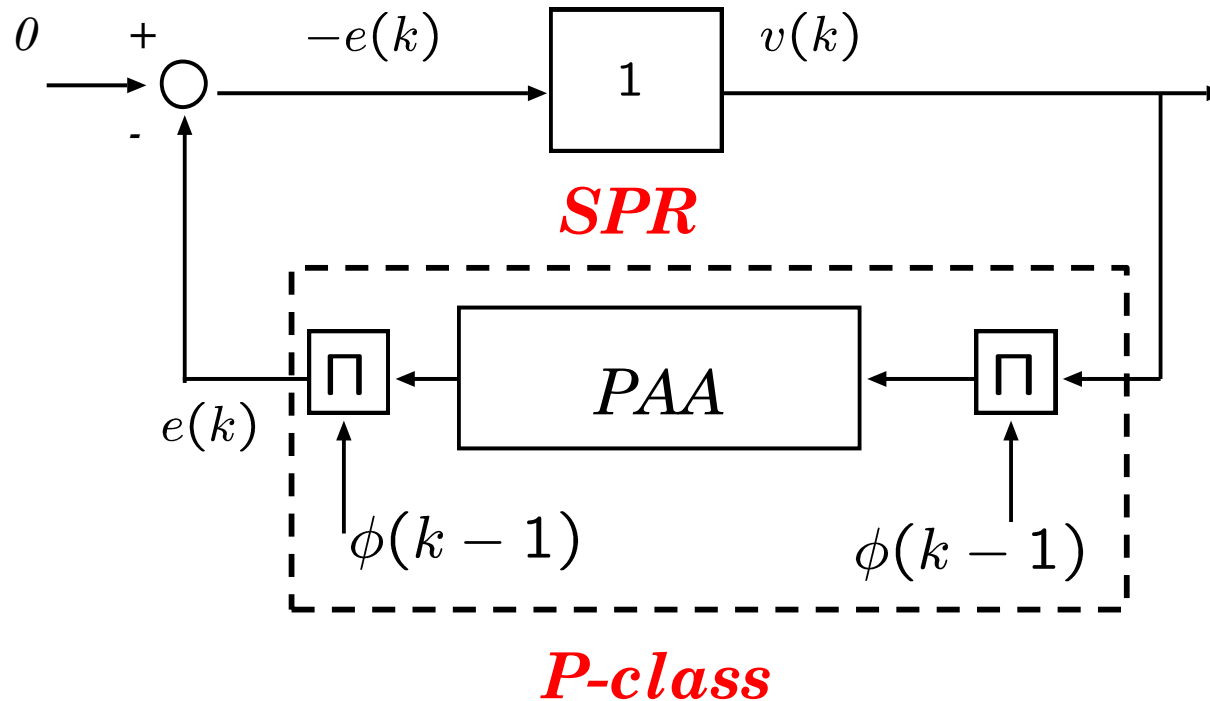
By the sufficiency portion of Asymptotic Hyperstability
Theorem:

$$|v(k)| \rightarrow 0$$

$$|e(k)| \rightarrow 0$$

Q.E.D.

Stability analysis of Series-parallel ID



By the sufficiency portion of Asymptotic Hyperstability Theorem:

$$|v(k)| \rightarrow 0$$

$$|e(k)| \rightarrow 0$$



How to we implement the PAA?

a-posteriori error & PAA:

$$e(k) = \phi^T(k-1)\tilde{\theta}(k)$$

$$\tilde{\theta}(k) = \tilde{\theta}(k-1) - F\phi(k-1)e(k)$$

} *Static coupling*

Solution: Use the a-priori error

$$e^o(k) = \phi^T(k-1)\tilde{\theta}(k-1)$$

How to we implement the PAA?

a-posteriori estimate & PAA:

$$e(k) = y(k) - \phi^T(k-1)\hat{\theta}(k)$$

$$\hat{\theta}(k) = \hat{\theta}(k-1) + F\phi(k-1)e(k)$$

} *Static coupling*

Solution: Use the a-priori error

$$\begin{aligned} e^o(k) &= y(k) - \phi^T(k-1)\hat{\theta}(\underline{k-1}) \\ &= \phi^T(k-1)\tilde{\theta}(\underline{k-1}) \end{aligned}$$

How to we implement the PAA?

$$\tilde{\theta}(k) = \tilde{\theta}(k-1) - F \phi(k-1)e(k)$$

Multiply by $\phi^T(k-1) = \phi_{k-1}^T$

$$\underbrace{\phi_{k-1}^T \tilde{\theta}(k)}_{e(k)} = \underbrace{\phi_{k-1}^T \tilde{\theta}(k-1)}_{e^o(k)} - \phi_{k-1}^T F \phi_{k-1} e(k)$$

$$e(k) = e^o(k) - \phi_{k-1}^T F \phi_{k-1} e(k)$$

Therefore,

$$e(k) = \frac{e^o(k)}{1 + \phi^T(k-1)F\phi(k-1)}$$

How we implement the PAA

1.
$$e^o(k) = y(k) - \phi^T(k-1)\hat{\theta}(k-1)$$
2.
$$e(k) = \frac{e^o(k)}{1 + \phi^T(k-1)F\phi(k-1)}$$
3.
$$\hat{\theta}(k) = \hat{\theta}(k-1) + F\phi(k-1)e(k)$$

Stability analysis of Series-parallel ID

We have shown that

$$e(k) \rightarrow 0$$

Now we will show that

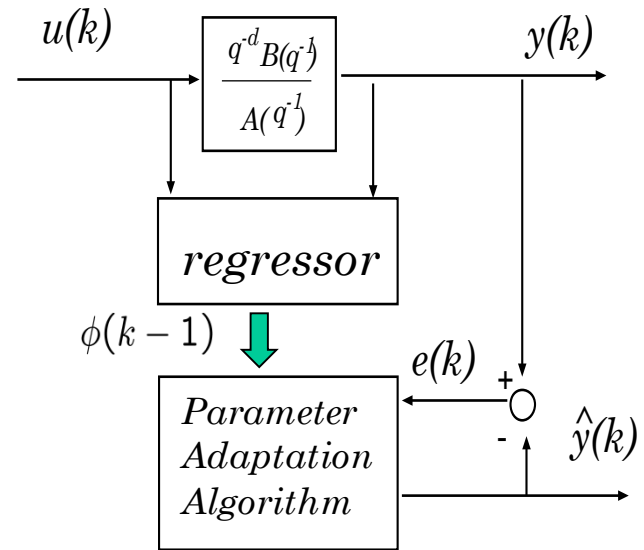
$$e^o(k) \rightarrow 0$$

Under the following assumptions:

$$|u(k)| < \infty \quad A(q^{-1}) \text{ is anti-Schur}$$

Since $y(k) = \frac{q^{-d}B(q^{-1})}{A(q^{-1})}u(k) \Rightarrow |y(k)| < \infty$

Since $\phi(k-1) = \begin{bmatrix} y(k-1) \\ \vdots \\ u(k-d) \\ \vdots \end{bmatrix} \Rightarrow \|\phi(k-1)\| < \infty$



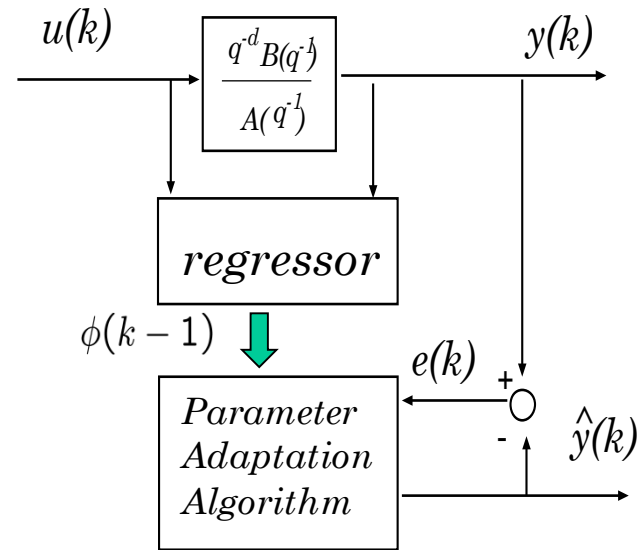
Stability analysis of Series-parallel ID

Thus, we know that

$$e(k) \rightarrow 0$$

$$\|\phi(k-1)\| < \infty$$

Remember that



$$e(k) = \frac{e^o(k)}{1 + \phi^T(k-1)F\phi(k-1)}$$

$$\Rightarrow e^o(k) = \underbrace{e(k)}_{\rightarrow 0} \underbrace{\{1 + \phi^T(k-1)F\phi(k-1)\}}_{< \infty}$$

$$\Rightarrow e^o(k) \rightarrow 0$$

Stability analysis of Series-parallel ID

We have shown that

$$e(k) \rightarrow 0 \quad e^o(k) \rightarrow 0$$

$$\|\phi(k-1)\| < \infty$$

What about the parameter error $\tilde{\theta}(k)$?

since

$$\underbrace{e^o(k)}_{\rightarrow 0} = \phi^T(k-1)\tilde{\theta}(k-1) \quad \Rightarrow \quad |\phi^T(k)\tilde{\theta}(k)| \rightarrow 0$$

However, this **does not imply** that the parameter error goes to zero

We need to impose another condition on $u(k)$ to guarantee that the parameter error goes to zero. (**persistence of excitation**)

